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VOLUME III

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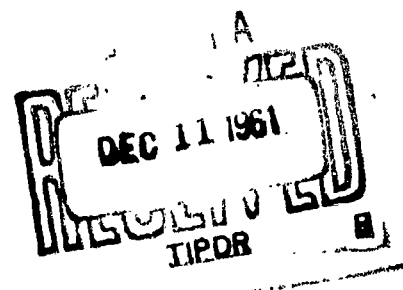
PASSIVE AERODYNAMIC ATTITUDE STABILIZATION OF NEAR EARTH SATELLITES

Volume III
MATHEMATICAL TECHNIQUES AND COMPUTER PROGRAM

O. C. JUELICH

NORTH AMERICAN AVIATION, INC.
COLUMBUS, OHIO

JULY 1961



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AERONAUTICAL SYSTEMS DIVISION

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MATHEMATICAL TECHNIQUES AND COMPUTER PROGRAM**

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JULY 1961

**FLIGHT DYNAMICS LABORATORY
CONTRACT Nr. AF 33(616)-7100
PROJECT Nr. 1366
TASK Nr. 13967**

**AERONAUTICAL SYSTEMS DIVISION
AIR FORCE SYSTEMS COMMAND
UNITED STATES AIR FORCE
WRIGHT-PATTERSON AIR FORCE BASE, OHIO**

**McGregor & Werner, Inc., Dayton, O.
400 - November 1961 - 10-342**

FOREWORD

The research reported herein was performed by North American Aviation, Inc., Columbus, Ohio for the Hypersonic Flight Section, Flight Branch of the Flight Dynamics Laboratory, Wright Air Development Division. The work was accomplished under Air Force Contract No. AF 33(616)-7100, Project No. 1366, Task No. 13967, "A Study of Aerodynamically Oriented and Stabilized Satellites." This research was carried out by the Engineering Research and Aerothermodynamics Development Groups of the Columbus Division, North American Aviation, Inc., with Dr. D. M. Schrello, Engineering Research Group, as Project Engineer. Mr. Joseph Ondrejka, Flight Dynamics Laboratory, was WADD Project Engineer.

The results of this study are reported in a series of three volumes of which this is Volume III. The other reports in this series are:

VOLUME I: "Librations due to Combined Aerodynamic and Gravitational Torques," by D. M. Schrello

VOLUME II: "Aerodynamic Analysis," by Paul H. Davison

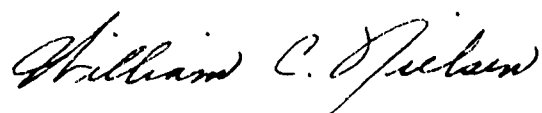
ABSTRACT

A computer program is presented which integrates numerically the pitch equation of an aerodynamically stabilized satellite. The mathematical theory of the linear second order equation with periodic coefficients and the integration procedure are discussed to clarify the structure and application of the program.

PUBLICATION REVIEW

This report has been reviewed and is approved.

FOR THE COMMANDER:



WILLIAM C. NIELSEN
Colonel, USAF
Chief, Flight Dynamics Laboratory

TABLE OF CONTENTS

	<u>Page No.</u>
INTRODUCTION.....	1
DISCUSSION	
1. DISCUSSION OF THE LINEAR SECOND ORDER DIFFERENTIAL EQUATION WITH PERIODIC COEFFICIENTS.....	3
1.1 General Case.....	3
1.2 Resonant Case.....	6
1.3 Stability Criteria.....	9
1.4 Short Term Boundedness.....	10
1.5 A "Built-In" Check on the Accuracy of the Numeric Integration.....	11
2. INTEGRATION PROCEDURE.....	12
2.1 Derivation of Predictor Formula.....	12
2.2 Corrector Formula.....	14
2.3 Integration Scheme.....	15
3. COMPUTER PROGRAM.....	17
3.1 Integration Portion of the Program.....	17
3.2 Card-Punching Portion of the Program.....	18
3.3 Atmospheric Properties Subroutine.....	19
3.4 A Potential Application.....	19
APPENDIX A - PROGRAM DESCRIPTION - PITCHING MOTION OF A SATELLITE.....	21
APPENDIX B - PROGRAM DESCRIPTION - ATMOSPHERE SUBROUTINE.....	51
APPENDIX C - PROGRAM DESCRIPTION - FIXED DECIMAL CARD READ ROUTINE WITH ERROR DETECTION.....	57
APPENDIX D - PROGRAM DESCRIPTION - PUNCH SCALING FUNCTION.....	61
APPENDIX E - PROGRAM DESCRIPTION - OUTPUT TAPE WRITE ROUTINE.....	65
APPENDIX F - SUMMARY OF LIBRARY ROUTINES.....	68
APPENDIX G - SAMPLE INPUT AND OUTPUT.....	69
BIBLIOGRAPHY.....	88

LIST OF SYMBOLS

A, B, C, D	Coefficients used in the derivation of Eq. (32)
a, b	Initial condition constants
a_n	The nth coefficient of Taylor's Series
F	Number of a card field
f	Function generated in the card-punch program
h	Altitude, increment in t
I	Identity matrix
i	Orbit inclination, Counting index
M	Inertia parameter
n	Counting index, integral multiplier
P, P_p, Q, Q_p	Aerodynamic parameters
r	Distance from center of earth
r_E	Mean radius of earth
S_n	Matrix defined in Eq. (22)
s	Constant appearing in error term of Taylor's series
t	Independent variable
V	Velocity of vehicle in inertial space
V_R	Velocity of vehicle relative to atmosphere
v	True anomaly of vehicle
W	Matrix whose determinant is the Wronskian of the system (y_1, y_2)
W	Wronskian of the system (y_1, y_2)
w	Eigenvalue bound for W , defined in Eq. (23)
w_p, w_1, w_2, w_3	Weighting constants in card-punch program
y	Solution of differential equation, Eqs. (5) or (6)
α	Angle of attack

α, β, γ	Periodic functions of t
Γ, Γ_q	Aerodynamic parameters
γ	Inclination of orbit to local horizontal
ϵ	Eccentricity, error
θ	Pitch angle relative to local horizontal
ρ	Atmospheric density
σ_{hi}	Eigenvalues of matrix S_n
ω_e	Earth rotation rate
ω	Eigenvalue of the matrix W

Subscripts (except counting indices)

e	even part
n	operator defined in Eq. (13)
o	odd part
p	perigee
p	periodic, calculated from predictor formula
s	calculated from Simpson's rule
0	particular solution
$1, 2$	homogeneous solution

Notation

\dot{x}	Derivative with respect to t
x'	Derivative with respect to ν
\bar{x}	Maximum magnitude, see Eq. (11)
x^*	An instance of x
Δx	An increment of x
$\frac{d}{dx}$	Differentiation
\cong	Approximate equality
\equiv	Identity

INTRODUCTION

The equation of satellite pitching motion derived in Volume I of this series of reports is:

$$\theta'' + 2Q\theta' + \{3M[1 - \epsilon \cos v] + P\}\theta = 2Q + \gamma P \quad (1)$$

where v , the true anomaly, is the independent variable,

θ is the pitch angle from the local horizontal,

ϵ is the orbital eccentricity,

M is the inertia ratio parameter,

and the remaining quantities are defined by the following relations:

$$\gamma = \frac{\epsilon \sin v}{1 + \epsilon \cos v}, \quad (2)$$

$$P = P_p (\rho/\rho_p) (V_R/V)^2 [1 + 2\epsilon(1 - \cos v)],$$

$$Q = Q_p (\rho/\rho_p) (V_R/V) [1 - \epsilon(1 - \cos v)] - \epsilon \sin v,$$

in which

$$(V_R/V) = 1 - (\omega_E / \dot{v}_p) \cos i,$$

$$\dot{v}_p = \frac{1}{r_p} \sqrt{\frac{\mu(1+\epsilon)}{r_p}}, \quad (3)$$

the subscript P denotes perigee conditions,

μ is the product of the universal gravitational constant and the mass of the earth,

ω_E is the Earth's rotation rate,

i is the orbit inclination,

ρ , the atmospheric density, is a tabular function of the altitude h , see for instance Minzner, (Ref. 1). The altitude h in turn is defined by

Manuscript released by the author February 1961 for publication as a WADD Technical Report.

$$h = r - r_E \quad (4)$$

with r_E the mean earth radius, and

$$r = r_p (1 + \epsilon) / (1 + \epsilon \cos v).$$

The quantities P_p , Q_p are defined by

$$P_p = \Gamma \rho_p r_p^2 / 2$$

$$Q_p = \Gamma_q \rho_p r_p / 8$$

where Γ is a pitching moment parameter, and

Γ_q is a damping in pitch parameter.

These parameters are defined and discussed in Volume I of this series of reports. It is desired to calculate θ and possibly the angle of attack $\alpha = \theta - \gamma$ for "all values" of the true anomaly.

Even though the differential equation is a linear second order equation it does not lend itself readily to solution in terms of elementary or tabulated functions particularly since the variation of density with altitude is a tabulated function. Direct numeric integration appears to offer a rather straightforward approach, provided its limitation to a finite range of v can be circumvented.

The means used to obtain results valid for all v constitute the first section of this report. The second section describes the method of numeric integration adopted. The final section discusses the computer program written to implement these results while the program itself is given in the appendices.

1. DISCUSSION OF THE LINEAR SECOND ORDER DIFFERENTIAL EQUATION WITH PERIODIC COEFFICIENTS

It is the purpose of this section of the report to show that three integrations carried out over one orbital period suffice to furnish information about the boundedness or stability of solutions of Eq. (1). Equations with arbitrary periodic coefficients are discussed to insure independence of the tabulated atmospheric density function. In this form the presentation is an amplification of the concise discussion given by Coddington and Levinson, (Ref. 2) and a minor extension as well since the reference discusses homogeneous equations only.

1.1 General Case

Let

$$\ddot{y} + \alpha \dot{y} + \beta y = \gamma \quad (5)$$

be a linear differential equation in which α , β , and γ are periodic functions of t , with common period of 2π . The dots denote differentiation with respect to t . Eq. (1) is of this type. Let

$$\ddot{y} + \alpha \dot{y} + \beta y = 0 \quad (6)$$

be the associated homogeneous equation. Now let y_0 be that solution of Eq. (5) that has

$$y_0(0) = 0, \quad \dot{y}_0(0) = 0$$

and let y_1, y_2 be solutions of Eq. (6) that have respectively

$$y_1(0) = 1, \quad \dot{y}_1(0) = 0,$$

$$y_2(0) = 0, \quad \dot{y}_2(0) = 1.$$

Since these solutions are obviously linearly independent, any solution of Eq. (5) may be written

$$y = y_0 + ay_1 + by_2. \quad (7)$$

For $t = 0, 2\pi$ Eq. (7) yields

$$\left. \begin{aligned} y(0) &= y_0(0) + a y_1(0) + b y_2(0) = a \\ \dot{y}(0) &= \dot{y}_0(0) + a \dot{y}_1(0) + b \dot{y}_2(0) = b \end{aligned} \right\}$$

$$\left. \begin{aligned} y(2\pi) &= y_0(2\pi) + a y_1(2\pi) + b y_2(2\pi) \\ \dot{y}(2\pi) &= \dot{y}_0(2\pi) + a \dot{y}_1(2\pi) + b \dot{y}_2(2\pi) \end{aligned} \right\} \quad (8)$$

If it is now required that y have period 2π ,

$$y(2\pi) = y(0), \quad \dot{y}(2\pi) = \dot{y}(0) \quad (9)$$

Eqs.(8) may be combined to yield

$$\left. \begin{aligned} y_0(2\pi) &= a [1 - y_1(2\pi)] - b y_2(2\pi) \\ \dot{y}_0(2\pi) &= -a \dot{y}_1(2\pi) + b [1 - \dot{y}_2(2\pi)] \end{aligned} \right\} \quad (10)$$

Let

$$W = \begin{bmatrix} y_1(2\pi) & y_2(2\pi) \\ \dot{y}_1(2\pi) & \dot{y}_2(2\pi) \end{bmatrix}$$

then Eq. (10) may be written

$$\begin{bmatrix} y_0(2\pi) \\ \dot{y}_0(2\pi) \end{bmatrix} = (I - W) \begin{bmatrix} a \\ b \end{bmatrix}$$

A unique periodic solution to Eq. (5) is thus seen to exist if $(I - W)$ is non-singular. It will be shown below that

$$\det(I - W) = 0$$

implies a resonance in the conventional sense. In the non-resonant case let the periodic particular solution be denoted by the subscript p :

$$y_p = y_0 + a y_1 + b y_2$$

where a and b are the solution to the system of equations given by Eqs. (10).

Now define the notation

$$\bar{y} = \max_{0 \leq t \leq 2\pi} (|y|). \quad (11)$$

Then

$$\bar{y}_p \leq \bar{y}_0 + |a| \bar{y}_1 + |b| \bar{y}_2,$$

and y_p exists and is bounded whenever y_0 , y_1 , y_2 , exist on the interval $[0, 2\pi]^p$, and $\det(I-W) \neq 0$.

Under these conditions, any solution of Eq. (5) may be written

$$y = y_p + a_0 y_1 + b_0 y_2 \quad (12)$$

where a_0 and b_0 are initial condition constants. The only change from Eq. (7) is the choice of the particular solution. The notation

$$t_n = t - 2n\pi \quad (13)$$

will be useful. In terms of the conditions at $t = 2n\pi$ Eq. (12) becomes

$$y(t) = y_p(t_n) + a_n y_1(t_n) + b_n y_2(t_n)$$

and in turn, when $t_n = 2\pi$,

$$\begin{aligned} y(2\pi + 2n\pi) &= y_p(2\pi) + a_n y_1(2\pi) + b_n y_2(2\pi) \\ &= y_p(0) + a_{n+1} y_1(0) + b_{n+1} y_2(0) = y_p(0) + a_{n+1}. \end{aligned}$$

Since $y_p(2\pi) = y_p(0)$,

$$a_{n+1} = a_n y_1(2\pi) + b_n y_2(2\pi).$$

Similarly

$$b_{n+1} = a_n \dot{y}_1(2\pi) + b_n \dot{y}_2(2\pi).$$

Thus

$$\begin{bmatrix} a_{n+1} \\ b_{n+1} \end{bmatrix} = W \begin{bmatrix} a_n \\ b_n \end{bmatrix} = W^{n+1} \begin{bmatrix} a_0 \\ b_0 \end{bmatrix}.$$

The solutions of Eq. (5) remain bounded if W^n remains bounded for all n . This in turn is the case if the magnitudes of the eigenvalues of W are at most 1. In this case an upper bound on the amplitude of solutions is

$$\bar{y} \leq \bar{y}_p + \sqrt{a_0^2 + b_0^2} (\bar{y}_1 + \bar{y}_2). \quad (14)$$

1.2 Resonant Case

If $(I - W)$ is singular, the system of equations

$$0 = (I - W) \begin{bmatrix} a \\ b \end{bmatrix} \quad (15)$$

has an infinity of non-trivial solutions. Let one of these be

$$a = a^*, \quad b = b^* \quad (16)$$

and let

$$y^* = a^* y_1 + b^* y_2. \quad (17)$$

Then Eq. (15) may be rewritten

$$0 = (I - W) \begin{bmatrix} a^* \\ b^* \end{bmatrix}$$

or

$$I \begin{bmatrix} a^* \\ b^* \end{bmatrix} = W \begin{bmatrix} a^* \\ b^* \end{bmatrix}$$

whence

$$\begin{bmatrix} y_1(0) & y_2(0) \\ \dot{y}_1(0) & \dot{y}_2(0) \end{bmatrix} \begin{bmatrix} a^* \\ b^* \end{bmatrix} = \begin{bmatrix} y_1(2\pi) & y_2(2\pi) \\ \dot{y}_1(2\pi) & \dot{y}_2(2\pi) \end{bmatrix} \begin{bmatrix} a^* \\ b^* \end{bmatrix},$$

so that

$$\begin{bmatrix} y^*(0) \\ \dot{y}^*(0) \end{bmatrix} = \begin{bmatrix} y^*(2\pi) \\ \dot{y}^*(2\pi) \end{bmatrix} . \quad (18)$$

Thus y^* is a non-trivial solution of period 2π of the homogeneous equation, Eq. (6). Since the period of y^* matches that of the forcing term of Eq. (5) this meets the accepted notions of resonance.

Conversely, if a solution of the homogeneous Eq. (6) satisfies Eq. (18) the argument may be reversed to show that Eq. (15) is valid.

In the resonant case, the system of equations, Eqs. (10), may or may not have a solution. If it does, the analysis for the non-resonant case applies, except that y_p is no longer unique. If, however, the system of equations, Eqs. (10) is inconsistent, no periodic solution of Eq. (5) exists. In this case let

$$y = y_0 + a_0 y_1 + b_0 y_2 \quad (19)$$

be some solution of Eq. (5), where a_0 and b_0 are again initial condition constants. By suitable choice of the initial condition constants Eq. (19) may be written

$$y(t) = y_0(t_n) + a_n y_1(t_n) + b_n y_2(t_n) \quad (20)$$

where t_n is defined in Eq. (13). Now

$$\begin{aligned} y(2\pi + 2n\pi) &= y_0(2\pi) + a_n y_1(2\pi) + b_n y_2(2\pi) \\ &= y_0(0) + a_{n+1} y_1(0) + b_{n+1} y_2(0) = a_{n+1} , \end{aligned}$$

and

$$\begin{aligned} \dot{y}(2\pi + 2n\pi) &= \dot{y}_0(2\pi) + a_n \dot{y}_1(2\pi) + b_n \dot{y}_2(2\pi) \\ &= \dot{y}_0(0) + a_{n+1} \dot{y}_1(0) + b_{n+1} \dot{y}_2(0) = b_{n+1} . \end{aligned}$$

Thus

$$\begin{bmatrix} a_{n+1} \\ b_{n+1} \end{bmatrix} = \begin{bmatrix} y_0(2\pi) \\ \dot{y}_0(2\pi) \end{bmatrix} + W \begin{bmatrix} a_n \\ b_n \end{bmatrix} ,$$

and, proceeding recursively

$$\begin{aligned}
 \begin{bmatrix} a_{n+1} \\ b_{n+1} \end{bmatrix} &= \begin{bmatrix} \gamma_0(2\pi) \\ \dot{\gamma}_0(2\pi) \end{bmatrix} + W \left(\begin{bmatrix} \gamma_0(2\pi) \\ \dot{\gamma}_0(2\pi) \end{bmatrix} + W \begin{bmatrix} a_{n-1} \\ b_{n-1} \end{bmatrix} \right) \\
 &= (I + W) \begin{bmatrix} \gamma_0(2\pi) \\ \dot{\gamma}_0(2\pi) \end{bmatrix} + W^2 \begin{bmatrix} a_{n-1} \\ b_{n-1} \end{bmatrix} \\
 &\dots = \left(\sum_{i=0}^n W^i \right) \begin{bmatrix} \gamma_0(2\pi) \\ \dot{\gamma}_0(2\pi) \end{bmatrix} + W^{n+1} \begin{bmatrix} a_0 \\ b_0 \end{bmatrix}.
 \end{aligned} \tag{21}$$

Now the vector $[a_{n+1}, b_{n+1}]$ can remain bounded as n increases only if the sum

$$S_n = \sum_{i=0}^{n-1} W^i \tag{22}$$

remains bounded.

Let σ_{ni} be the eigenvalues of S_n and ω_i be those of W , where $i = 1, 2$. The eigenvalues of the matrix polynomial, Eq. (22) have the relation

$$\begin{aligned}
 \sigma_{ni} &= (1 - \omega_i^n) / (1 - \omega_i), & \omega_i &\neq 0, 1 \\
 &= 0, & \omega_i &= 0 \\
 &= n, & \omega_i &= 1
 \end{aligned}$$

Thus, the definition

$$w = \max(|\omega_1|, |\omega_2|) \tag{23}$$

and relation

$$0 < w < 1 \tag{24}$$

imply

$$|\sigma_{ni}| \rightarrow |1/(1-w_i)| < 1/(1-w) \quad \text{as } n \rightarrow \infty.$$

But if the relation, Eq. (24), is satisfied the second term of Eq. (21) is also bounded, and the amplitude of y is limited to

$$|y| \leq \frac{1}{1-w} \sqrt{\gamma_0(2\pi)^2 + \dot{\gamma}_0(2\pi)^2} + (\bar{\gamma}_1 + \bar{\gamma}_2) \sqrt{a_0^2 + b_0^2} \quad (25)$$

where the bars are defined in Eq. (11).

The derivation of the bound, given by Eq. (25), did not use the fact of resonance, thus it is applicable even to the non-resonant case, although in the latter case the bound given by Eq. (14) will usually be sharper. (It should be borne in mind that the symbols a_0 and b_0 have different significances in the two expressions.)

1.3 Stability Criteria

The eigenvalues of the matrix W satisfy the equation

$$0 = \begin{vmatrix} \omega - \gamma_1(2\pi) & -\gamma_2(2\pi) \\ -\dot{\gamma}_1(2\pi) & \omega - \dot{\gamma}_2(2\pi) \end{vmatrix} = \omega^2 - [\gamma_1(2\pi) + \dot{\gamma}_2(2\pi)]\omega + \det W$$

so that

$$\omega = \frac{\gamma_1(2\pi) + \dot{\gamma}_2(2\pi)}{2} \pm \sqrt{\left[\frac{\gamma_1(2\pi) + \dot{\gamma}_2(2\pi)}{2} \right]^2 - \det W} \quad (26)$$

When the eigenvalues are complex, they are conjugates, so

$$\begin{aligned} \omega_1 \omega_2 &= \left[\frac{\gamma_1(2\pi) + \dot{\gamma}_2(2\pi)}{2} \right]^2 - \det W - \left[\frac{\gamma_1(2\pi) + \dot{\gamma}_2(2\pi)}{2} \right]^2 \\ &= \det W, \end{aligned}$$

and thus

$$|\omega_1| = \sqrt{\det W}.$$

When the eigenvalues are real, let the one larger in absolute value be ω_1 . Then

$$|\omega_1| \geq \left| \frac{y_1(2\pi) + \dot{y}_2(2\pi)}{2} \right| \geq \sqrt{\det W}.$$

For bounded motions, therefore, it is necessary that

$$\det W \leq 1.$$

It is to be noted that $\det W$ is the Wronskian of the system (y_1, y_2) , evaluated at $t = 2\pi$. Abel's formula for the Wronskian is:

$$W(x) = W(0) e^{\int_0^x \alpha(t) dt},$$

Thus

$$\det W = W(2\pi) = \begin{vmatrix} y_1(0) & y_2(0) \\ \dot{y}_1(0) & \dot{y}_2(0) \end{vmatrix} e^{\int_0^{2\pi} \alpha(t) dt} = e^{\int_0^{2\pi} \alpha(t) dt}.$$

Now if α is identically zero, or even if it has an average value of zero on the interval $(0, 2\pi)$,

$$\det W = 1.$$

Then, referring to Eq. (23),

$$w \geq 1.$$

It may be concluded, therefore, that in the absence of the damping term, the resonant solutions are unbounded unless Eqs. (10) happen to be dependent. The non-resonant solutions were shown above, Eq. (14), to be bounded, unless $w > 1$.

1.4 Short Term Boundedness

In the application of the results obtained above to Eq. (1) it must be recalled from Volume I, Appendix C of this series of reports, that the constants (or elements) describing the orbit are themselves subject to drift as the orbit decays. Thus the results are applicable to some large but finite number of periods. Under such a limitation an ultimately unbounded motion

may still be acceptable if its rate of growth is small. For the n th period the bound expressed by Eq. (25) may be written:

$$\bar{y}(t_{n+1}) \leq \frac{\omega^n - 1}{\omega - 1} \sqrt{y_0(2\pi)^2 + \dot{y}_0(2\pi)^2} + \omega^{n-1} (\bar{y}_1 + \bar{y}_2) \sqrt{y(0)^2 + \dot{y}(0)^2} \quad (27)$$

while in the non-resonant case the bound given by Eq. (14) becomes

$$\bar{y}(t_{n+1}) \leq \bar{y}_p + \omega^{n-1} \sqrt{[y_p(0) - y(0)]^2 + [\dot{y}_p(0) - \dot{y}(0)]^2}. \quad (28)$$

Now the total lifetime of the satellite may be divided into regions during each of which the parameters of the orbit may be considered constant, and during each of which the growth or decay of the pitch amplitude may be estimated by means of Eq. (27), or in a non-resonant case by Eq. (28).

1.5 .A "Built-In" Check on the Accuracy of the Numeric Integration

Let Eq. (5) have a unique periodic solution y_p and let

$$y_p = y_e + y_o$$

where y_e is the even part of y_p and y_o is the odd part of y_p . Further, suppose that in Eq. (5) the functions α and γ are odd functions of t , and β is an even function of t . Then Eq. (5) becomes

$$(\ddot{y}_e + \alpha \dot{y}_e + \beta y_e) + (\ddot{y}_o + \alpha \dot{y}_o + \beta y_o) = \gamma.$$

The parity properties of functions guarantee that the first parenthesis on the left is an even function of t , while the second parenthesis is an odd function. Since the right member is an odd function, the first parenthesis must vanish. If there existed a non-trivial even function y_e the uniqueness of y_p would be destroyed. Thus

$$y_e \equiv 0,$$

and y_p is an odd function, so that $y_p(0) = 0$. Then in the solution of Eqs. (10):

$$a = 0,$$

and

$$y_p = y_o + b y_1.$$

This situation arises in Eq. (1) when the damping in pitch parameter, Γ_q , vanishes. In this case the size of a computed from Eqs. (10) becomes a measure of the accuracy of the numeric integration used to obtain the coefficients in these equations.

2. INTEGRATION PROCEDURE

The choice of integration procedure involves a balance between accuracy, speed, stability, and auxiliary "housekeeping" requirements. Gill, (Ref. 3) has derived a very elegant version of the Runge-Kutta fourth order procedure in which the housekeeping is minimized, in that only one storage cell need be assigned to each variable to be integrated. Milne (Ref. 4, Section 38) earlier gave a predictor-corrector method which obtains the same accuracy with half as many substitutions into the differential equation, but requires that a history of past values of the variables be kept. Milne's predictor formula requires a history of four previous values of the derivative, and if it is desired to double the step-size in the course of the integration a history of seven previous values must be available, along with a record of the time at which the step size was last doubled. The starting procedure for the predictor-corrector method is necessarily relatively involved. Since the corrector formula, Simpson's Rule, requires a history of only two previous values, it would be desirable to have a predictor formula with an equally short time-base, even at the cost of some accuracy and stability. Milne (Ref. 4, Sections 30 and 31) gives a procedure for deriving such formulas to arbitrary specifications and for estimating their accuracy. The procedure is here used to obtain the desired formula.

2.1 Derivation of Predictor Formula

In the identity:

$$y(t_0 + h) - y(t_0 - h) = \int_{t_0 - h}^{t_0 + h} \dot{y} dt \quad (29)$$

the assumption that the second term on the right is a linear combination of $y(t_0)$, $y(t_0 - h)$, $h\dot{y}(t_0)$ and $h\dot{y}(t_0 - h)$, may be written

$$\int_{t_0 - h}^{t_0 + h} \dot{y} dt = A y(t_0) + B y(t_0 - h) + C h \dot{y}(t_0) + D h \dot{y}(t_0 - h). \quad (30)$$

The coefficients A, B, C, D may be determined by requiring that Eq. (30) be exact for the first four terms of the Taylor expansion of about . Thus, let

$$y(t) = a_0 + a_1(t - t_0) + a_2 \frac{(t - t_0)^2}{2} + a_3 \frac{(t - t_0)^3}{6} + \dots \quad (31)$$

where

$$a_n = \frac{d^n y(t_0)}{dt^n}.$$

Substitution of Eq. (31) into Eq. (29) and Eq. (30) gives respectively

$$\int_{t_0-h}^{t_0+h} \dot{y} dt \cong 2a_1 h + \frac{1}{3} a_3 h^3,$$

$$\begin{aligned} \int_{t_0-h}^{t_0+h} \dot{y} dt \cong & A a_0 + B (a_0 - a_1 h + \frac{a_2}{2} h^2 - \frac{a_3}{6} h^3) \\ & + C a_1 h + D (a_1 h - a_2 h^2 + \frac{a_3}{2} h^3). \end{aligned}$$

Equating the coefficients of a_0 , a_1 , a_2 , and a_3 respectively, yields:

$$\left. \begin{aligned} A + B &= 0 \\ C + D - B &= 2 \\ \frac{1}{2} B - D &= 0 \\ \frac{1}{2} D - \frac{1}{6} B &= \frac{1}{3} \end{aligned} \right\}.$$

The solution to this system is

$$A = -4, \quad B = 4, \quad C = 4, \quad D = 2.$$

Then Eq. (30) becomes

$$\int_{t_0-h}^{t_0+h} \dot{y} dt \cong -4y(t_0) + 4y(t_0-h) + 4h\dot{y}(t_0) + 2h\dot{y}(t_0-h),$$

which yields in Eq. (29):

$$\begin{aligned} y(t_0+h) &\cong y(t_0-h) + 4 \left\{ y(t_0-h) - y(t_0) + \frac{h}{2} [\dot{y}(t_0-h) + 2\dot{y}(t_0)] \right\} \\ &= y_p(t_0+h) \end{aligned} \quad (32)$$

where the subscript p stands for "predicted value". Its derivation insures that Eq. (32) is exact to third order terms.

The Taylor series, Eq. (31) may be made exact by including the residue term:

$$y(t) = a_0 + a_1(t-t_0) + a_2 \frac{(t-t_0)^2}{2} + a_3 \frac{(t-t_0)^3}{6} + \frac{d^4 y(s)}{dt^4} \cdot \frac{(t-t_0)^4}{24} \quad (33)$$

where s is on the interval $[t_0, t]$.

Now the error committed by the use of $y_p(t_0+h)$ in place of $y(t_0+h)$ may be obtained by subtracting the right member of Eq. (32) from its left member. If each term in this difference is expressed in terms of Eq. (33) or its first derivative, the coefficients of a_0 , a_1 , a_2 , and a_3 will be zero because Eq. (32) is accurate to third order terms. The residue terms will remain:

$$y(t_0+h) - y_p(t_0+h) = \frac{h^4}{24} \left[\frac{d^4 y(s_1)}{dt^4} - 5 \frac{d^4 y(s_2)}{dt^4} + 8 \frac{d^4 y(s_3)}{dt^4} \right],$$

where s_1 is between t_0 and t_0+h , while s_2 and s_3 are between t_0 and t_0-h . The three distinct values arise from the fact that s in Taylor's Theorem, Eq. (33), cannot be expected to be the same for the expansions of $y(t_0+h)$, $y(t_0-h)$, and $\dot{y}(t_0-h)$. However, Eq. (32) may be shown to satisfy Milne's Theorem 2, (Ref. 4, Section 31) which in effect permits the replacement of s_1 , s_2 , and s_3 by a single s between t_0-h and t_0+h . The error becomes

$$\frac{d^4 y(s)}{dt^4} \cdot \frac{h^4}{6},$$

and Eq. (32) may be rewritten:

$$y(t_0+h) = y(t_0-h) + 4 \left\{ y(t_0-h) - y(t_0) \right. \\ \left. + \frac{h}{2} [\dot{y}(t_0-h) + 2\dot{y}(t_0)] \right\} + \frac{d^4 y}{dt^4} \cdot \frac{h^4}{6}. \quad (34)$$

2.2 Corrector Formula

Simpson's rule is

$$y(t_0+h) \approx y(t_0-h) + \frac{h}{3} [\dot{y}(t_0-h) + 4\dot{y}(t_0) + \dot{y}(t_0+h)] = y_s(t_0+h) \quad (35)$$

where the subscript s denotes "calculated from Simpson's rule". An error analysis for Simpson's rule yields

$$y(t_0+h) = y(t_0-h) + \frac{h}{3} [\dot{y}(t_0-h) + 4\dot{y}(t_0) + \dot{y}(t_0+h)] - \frac{d^5 y}{dt^5} \cdot \frac{h^5}{90}. \quad (36)$$

In the derivation of the error term in Eq. (35) the assumption was made that the other terms on the right-hand side are known precisely. If this assumption

is replaced by the assumption that $\dot{y}(t_0+h)$ was itself computed by Eq. (32) the error term is larger, in fact

$$y(t_0+h) = y(t_0-h) + \frac{h}{3} [\dot{y}(t_0-h) + 4\dot{y}(t_0) + \dot{y}_p(t_0+h)] + 4 \frac{d^5 y}{dt^5} \cdot \frac{h^5}{90} \quad (37)$$

If, however, $\dot{y}_s(t_0+h)$ is used in place of $\dot{y}(t_0+h)$ the error term is about

$$\frac{6}{5} \cdot \frac{d^5 y}{dt^5} \cdot \frac{h^5}{90}.$$

2.3 Integration Scheme

The predictor-corrector scheme is then:

- a) With $y = \theta'$ use Eq. (34) to predict $\theta'(v+\Delta v)$ from $\theta'(v)$, $\theta'(v-\Delta v)$, $\theta''(v)$, $\theta''(v-\Delta v)$.
- b) With $y = \theta$ use Eq. (36) to predict $\theta(v+\Delta v)$ from $\theta(v-\Delta v)$, $\theta'(v-\Delta v)$, $\theta'(v)$ and the predicted $\theta'(v+\Delta v)$.
- c) Use the predicted $\theta(v+\Delta v)$ and $\theta'(v+\Delta v)$ in Eq. (1) to predict $\theta''(v+\Delta v)$.
- d) Use the predicted $\theta''(v+\Delta v)$ in Eq. (35) with $y = \theta'$ to calculate the corrected $\theta'(v+\Delta v)$.
- e) Use the corrected $\theta'(v+\Delta v)$ in Eq. (35) with $y = \theta$ to calculate the corrected $\theta(v+\Delta v)$.
- f) Use the corrected $\theta(v+\Delta v)$ and $\theta'(v+\Delta v)$ in Eq. (1) to calculate the corrected $\theta''(v+\Delta v)$.

The small size of the error term in Eq. (36) makes it unlikely that an iteration of steps d, e, f would improve the result, if the prediction of steps a, b, c is at all adequate. This adequacy may be tested by comparing the predicted and corrected values of $\theta''(v+\Delta v)$. Since the error estimates for the prediction exceed those for the correction the difference between predicted and corrected values is a pessimistic estimate of the error incurred at each step of the integration. Let $\epsilon(\Delta v)$ be the magnitude of the difference between the predicted and corrected values of $\theta''(v+\Delta v)$, and let $\bar{\epsilon}$ be the maximum tolerable difference. Then if

$$\epsilon(\Delta v) \leq \bar{\epsilon}/32$$

the error estimates for Eq. (35) suggest that

$$\epsilon(2\Delta v) \leq \bar{\epsilon}.$$

Thus a sufficiently small ϵ justifies a doubling of the step size. If, however

$$\epsilon(\Delta v) > \bar{\epsilon}$$

the integration must be restarted with a smaller value of Δv .

Starting, as well as restarting may be accomplished by Taylor's formulas

$$\theta'(v + \Delta v) = \theta'(v) + \theta''(v)\Delta v + \frac{d^3\theta(s)}{dv^3} \cdot \frac{(\Delta v)^2}{2}, \quad (38)$$

$$\theta(v + \Delta v) = \theta(v) + \theta'(v)\Delta v + \theta''(v)\frac{(\Delta v)^2}{2} + \frac{d^3\theta(s)}{dv^3} \cdot \frac{(\Delta v)^3}{6}, \quad (39)$$

where s is between v and $v + \Delta v$. The relatively low powers of Δv appearing in the error terms of Eq. (38) and (39) suggest that small values of Δv be used to retain accuracy. Since the predictor-corrector scheme makes it easy to double the step size there is but small penalty for setting the initial value of Δv too small.

Computational experiments have been conducted comparing the procedure presented above with Gill's version (Ref. 3) of the Runge-Kutta fourth order procedure and with the Kutta fourth order formula as quoted by Milne (Ref. 5). All three processes gave essentially the same accuracy for the same step size; as mentioned above, the present process requires half as many substitutions into the differential equation. It should, however, be noted that the relatively large coefficients appearing in Eq. (34) tend to favor the build up of "inherited" errors, so that the present method cannot be expected to be as stable as the Runge-Kutta process for differential equations with unstable solutions.

The potential build-up of inherited error is not of concern in the present study for three reasons. Firstly, the range of integration is relatively short so that inherited error cannot build up very far. Secondly, the most critical cases are the most unstable cases, but in these the demonstration of instability is obvious. Thirdly, application of the accuracy criterion developed in Section 1.5 to the computer results justifies, a posteriori, the assertion that the error build-up was nil to four decimal places.

3. COMPUTER PROGRAM

Program Descriptions of the various components of the Computer Program written to calculate solutions of Eq. (1) are included in Appendices A to F. Sample input and output data are in Appendix G. The program has been checked out and used at the North American Aviation, Inc. Columbus IBM 704 computing installation to generate the numerical results discussed in Volume I of this series of reports. Certain systems features of this program, such as the choice of input medium (magnetic tape or punch-cards), assignment of magnetic tape unit numbers, labelling of library routines, etc. may have to be varied if this program is to operate successfully at other installations or on other computing machines. It is believed that the information furnished is adequate to enable anyone familiar with the IBM Fortran Manuals (for instance Ref. 6 and 7), and the operating system of his installation to adapt the source language deck to that installation.

The program was written in two portions. The first portion integrates the differential equation, Eq. (1), and its homogeneous part, and records the results on a magnetic tape as well as on the output medium. The second portion reads the magnetic tape and produces punched cards suitable for automatic plotting. The portions are discussed separately below and a brief discussion of the atmosphere table look-up routine is also given. This section concludes with some remarks on a potential application of the computer program.

3.1 Integration Portion of the Program

All input data is read by means of a "sparse data" routine so that information unchanged from one case to the next need not be written or key-punched repetitively. The only item of input data modified by the program is the identification number used to identify records on the intermediate storage tape, which is automatically advanced from record to record. To further facilitate the preparation of input data the primary input variables are presented in lists; the program systematically uses each combination of list entries. All angles in input and output are expressed in degrees; however, inside the computer and on the intermediate storage tape they are carried in radian units.

In the integration of the differential equations care is taken to provide common abscissas from one integration to the next. This is accomplished by using a computing interval obtained from the print interval by successive halving, and by not doubling the step size (when doubling is permitted by the criteria of Section 2) if this would cause the end of the print interval to fall inside a computing interval. The accuracy of the integration is further insured by a test which aborts the calculation if the step size does not expand in the first three intervals. If the step size fails to expand, the accuracy of the starting formulas Eqs. (38), (39) is less than that implied by the predictor-corrector method. The calculation should be attempted again with a smaller minimum step size. The integration is also aborted if the magnitude of any of the θ 's exceeds 10^7 , such an event would imply a gross data error, or a machine failure. The number of computing steps taken during

each print interval is printed out so that the step size used may be deduced, the total number of steps for each integration is printed out as an aid to future computing time estimates. As compiled for the IBM 704, the program will integrate about 8.5 steps per second.

3.2 Card-Punching Portion of the Program

This section may be combined with the first section in a single computer run, or it may be used separately if the intermediate storage tape is saved from run to run. The second option permits inspection and editing of the curves to be punched into cards. Since the on-line punching of cards is a relatively expensive process the card format was designed to admit up to fifteen curves per card deck, while retaining complete flexibility as to size and placement of the plots. This portion also reads its input data (specifying the editing information) with the "sparse data" routine. The only input item modified by the program is the card deck identification number which serves as a signal that all information to be punched has been accumulated. This number is reset to zero after the card deck has been punched to indicate that the store of information is again incomplete.

The punched-card output for automatic plotting assumes a plotting device capable of accepting one coordinate pair per card. Abscissa and ordinate may be placed in any of sixteen four digit fields, or the abscissa may be suppressed in favor of an abscissa punched for another curve. The abscissa field will contain the independent variable ψ . The ordinate may contain any function of the form

$$f = |\omega_p| \theta_0 + \omega_1 \theta_1 + \omega_2 \theta_2 + \omega_\gamma \gamma$$

where θ_0 is the particular solution of Eq. (1) corresponding to γ_0 of Section 1,

θ_1, θ_2 are the solutions of the homogeneous part of Eq. (2) corresponding to γ_1, γ_2 of Section 1,

γ is defined in Eq. (2)

and the ω 's are input data.

For $\omega_\gamma = 0, \omega_p = 1, f$ will be a solution of the differential equation, Eq. (1). When $\omega_\gamma = -1, f$ will be the angle of attack, α . When $\omega_p = -1$, the input values of ω_1 and ω_2 will be ignored, instead the program will use the pre-computed values needed to make f periodic, of orbital period.

The card decks produced will contain, in addition to the abscissa-ordinate pairs, four terminating cards. The first two of these are calibration check cards which will position the plotting head to the lower left hand and upper right hand corners of the plot respectively, the third contains an 11-punch in Column 1 which may be used to stop the plotting device, and the fourth is completely blank, serving as a separator between decks. The body of the deck, and the first two terminating cards have a 0-punch in Column 1, sequence number in Columns 5-8, and a deck identification number in Columns 2-4. The four

digit fields consisting of Columns 9-12, 13-16, etc to 69-72 are numbered $F = 1, 2, \dots, 16$ respectively and are the data fields proper (Columns 73-80 are not readily accessible to the IBM 704 computer).

The tape file of data is searched completely for the record required by the input data, so that in principle these records could be demanded in any order. The search is most efficient however if the records are demanded in the order in which they are stored on the tape.

3.3 Atmospheric Properties Subroutine

The atmospheric properties routine used in the program is capable of simulating atmosphere tables based on the ideal gas law and on linear variations of temperature, gas constant, and specific heat ratio with geopotential altitude. In the present program the routine was used to obtain the density distribution of the 1959 ARDC (Minzner) Atmosphere, (Ref. 1), which was represented by use of the Molecular Scale Temperature in place of the usual temperature. The detail input data are given in Appendix G.

3.4 A Potential Application

In its present form the program can furnish information about the stability in pitch of a given satellite in a given orbit. If the detailed motion is not of interest, only the first portion of the program is required. For a design study, knowledge of the stability boundaries in various parameter planes of the differential equation, Eq. (1), would be desirable. These occur when the magnitude of the larger eigenvalue ω given by Eq. (26) passes through the value 1. With minor modifications the subroutine INTEG of the first part of the present computer program could be used as the basis of a program to search iteratively for these stability boundaries. Points of departure for these searches could be obtained from the eigenvalues of the sine problem to which the present problem reduces itself when the orbital eccentricity is zero.

A NOTE ON THE APPENDICES

Appendices A to E are presented in the format of a standard SHARE program description.

APPENDIX A

PROGRAM DESCRIPTION - PITCHING MOTION OF A SATELLITE
NORTH AMERICAN AVIATION, INC. COLUMBUS
ENGINEERING PROGRAM DESCRIPTION

1. Identification

- a. Pitching Motion of a Satellite, IM 091
- b. O. C. Juelich, December 1960
- c. Research Group - 350
- d. Fortran Source Deck is up to date.

2. Purpose

Numerically integrates one particular and two homogeneous solutions of the pitch-equation. Solutions are printed, and optionally punched into cards in scaled form suitable for automatic plotting.

3. Restrictions

- a. Uses Tape 5 as input tape
 Tape 6 as printer output tape
 Tape 2 for intermediate storage of results
 Tape 7 to store part of the program
- b. Operates in N.A.A. monitor for IBM 704 Fortran

4. Method

- a. The mathematical method is described in Report WADD TR 61-133 Vol. III, of which this description is a part.
- b. The program is designed to terminate calculations if the step size has not adequately expanded in the first three print intervals or if any of the solutions exceed 10 million degrees in amplitude.
- c. Punched Card output is described in Section 3.2 of this report.

5. Use

The program consists of two parts. The first part generates solutions of the differential equation and records these on magnetic tape. The second part retrieves selected solutions and scales them for automatic plotting. The two parts can be combined in one machine run or they can be used on separate occasions if the intermediate storage tape (tape 2) is preserved. The latter alternative permits inspection of the printed results before card-punching is undertaken.

6. Coding Information

- a. The first part consists of a main program and two subroutines labeled INTEG, DIFFC. In addition subroutine ATMPS (1F113) and Utility File

subroutine FXRCH are used, as well as Library subroutines SQRT, COS, SIN, CHAIN, and Fortran system routines.

- b. The second part is Chain 1 on Tape 7. It consists of a main program and a subroutine labelled SCALE. In addition Utility File Subroutines FXRCH, NPSCL, WRITE, are used, along with Fortran system routines.
- c. Descriptions of subroutines ATMOS, FXRCH, NPSCL, and WRITE are given separately.

7. Input Data

- a. All input data to both parts of the program is read by the Utility File Routine FXRCH into the Fortran COMMON Data Region.
- b. Part one requires the following data:

<u>Location</u>	<u>Symbol</u>	<u>Designation, Description</u>
7	dv_{min}	Minimum computing step size bound, degrees The minimum computing step size is the largest number of the form $dv_{print}/2^n$ (n integral) and $\leq dv_{min}$
9	dv_{print}	Print Interval, degrees Should be a factor of 360° .
28	RECID	Record Identification Number or Control Number. If this number is negative or zero the remaining data set is ignored. If RECID is negative part II is loaded and given control. If RECID is zero tape 2 is rewound and computation ends. If RECID is positive it becomes the identification number of the data case, if it is omitted the value of RECID from the previous data case increased by 1. is used.
30	r_E	Radius of Earth, feet Used in Eq. (4), but not in subroutine ATMOS.
31	μ	Product of Universal gravitational constant and mass of earth, ft^3/sec^2 Used in Eq. (3).
32	TEL	Table used for routine ATMOS (1F113) See Appendix B.

<u>Location</u>	<u>Symbol</u>	<u>Designation, Description</u>
201	n_i	Number of orbit inclinations,
202	i_1	first orbit inclination, degrees
203	i_2	second orbit inclination
et seq.		
211	n_h	Number of perigee altitudes,
212	h_1	first perigee altitude, feet
213	h_2	second perigee altitude
et seq.		
221	n_e	Number of eccentricities,
222	e_1	first eccentricity, dimensionless
223	e_2	second eccentricity
et seq.		
231	n_r	Number of pitching moment parameters,
232	r_1	first pitching moment parameter
233	r_2	second pitching moment parameter
et seq.		
241	n_{r_q}	Number of damping in pitch parameters
242	r_{q1}	first damping in pitch parameter
243	r_{q2}	second damping in pitch parameter
et seq.		
251	n_M	Number of inertia ratio parameters
252	M_1	first inertia ratio parameter
253	M_2	second inertia ratio parameter
et seq.		

The $n_i, n_h, n_e, n_r, n_{r_q}, n_M$ combinations of the listed values of i, h, e, r, r_q, M will be used systematically. The results will be identified by successive values of RECID.

c. Part two requires the following data:

<u>Location</u>	<u>Symbol</u>	<u>Designation, Description</u>
1.	RECID	Identification number of tape record to be plotted.
2.	w_p	Weight of function θ_0 in curve to be plotted Should be 1, 0, or -1.
3.	w_γ	Weight of $\gamma(v)$ in curve to be plotted Should be 0 or -1.
4.	w_1	Weight of function θ_1 in curve to be plotted Ignored when $w_p = -1$.
5.	w_2	Weight of function θ_2 in curve to be plotted Ignored when $w_p = -1$.

<u>Location</u>	<u>Symbol</u>	<u>Designation, Description</u>
6.	f_{min}	Minimum value of function in plotting interval, degrees If f is less than this value the point will be plotted on the bottom margin of the paper.
7.	C_{min}	Plotter counts for f_{min} .
8.	f_{max}	Maximum value of function in plotting interval, degrees If f exceeds this value the point will be plotted on the top margin of the paper.
9.	C_{max}	Plotter counts for f_{max} .
10.	C_{edge}	Plotter counts for top margin of the paper. The bottom margin is at zero counts.
11.	F_f	Number of the card field in which f is to appear. Should be between 1. and 16.
12.	v_{min}	Minimum value of v in plotting interval, degrees If v is less than this value the point will be plotted on the left margin of the paper.
13.	d_{min}	Plotter counts for v_{min}
14.	v_{max}	Maximum value of v in plotting interval, degrees. If v exceeds this value the point will be plotted on the right margin of the paper.
15.	d_{max}	Plotter counts for v_{max}
16.	d_{edge}	Plotter counts for right margin of the paper. The left margin is at zero counts.
17.	F_v	Number of the card field in which v is to appear, or control number. If F_v is zero, v will not be entered on the punched cards.
18.	CID	Identification number for card deck to be punched, or control number. If CID is zero the scaled data are accumulated in core storage for later punching.

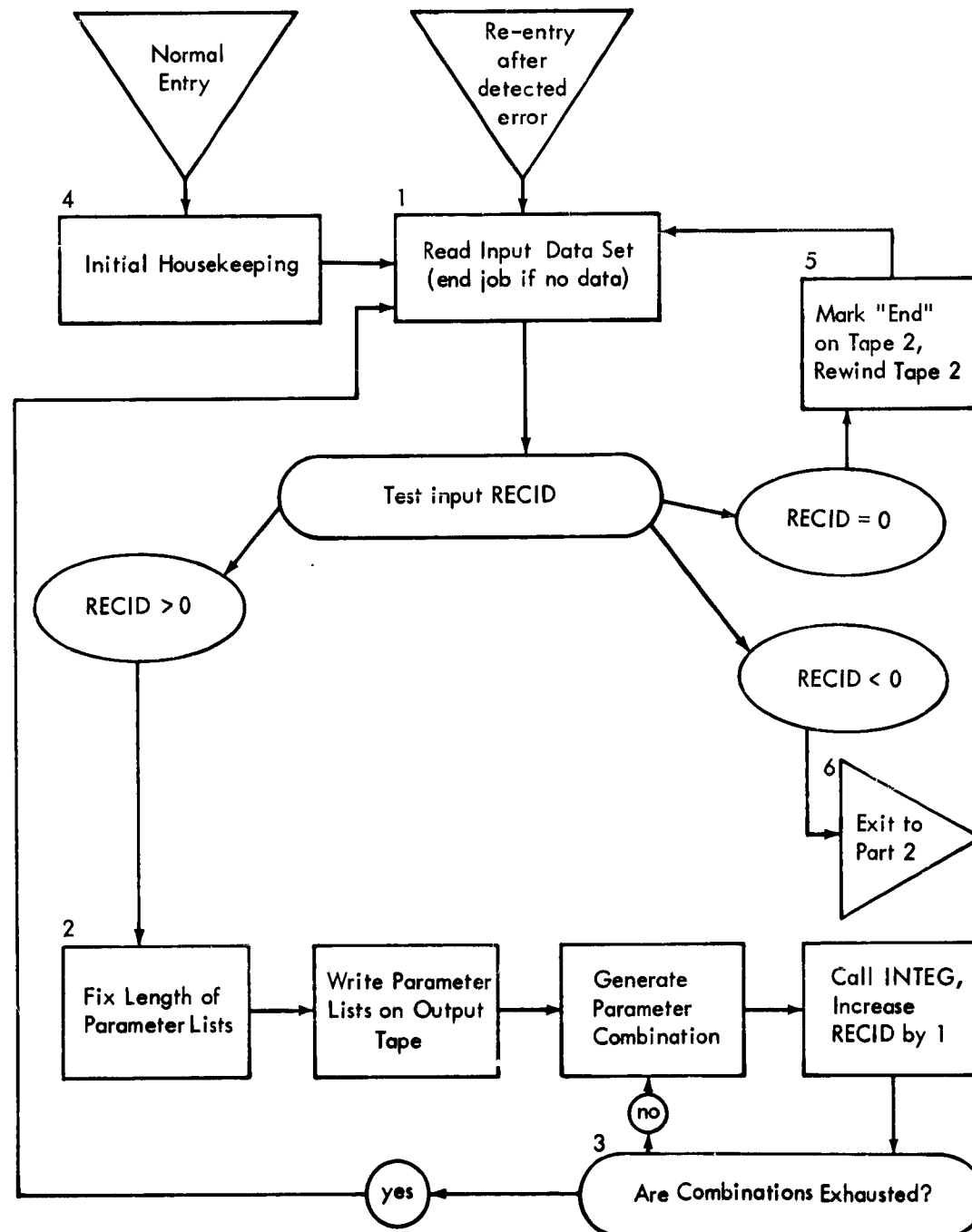
<u>Location</u>	<u>Symbol</u>	<u>Designation, Description</u>
-----------------	---------------	---------------------------------

If CID is not zero the accumulated information is punched into cards and CID becomes an identification number in columns 2 to 4 of each card. After punching CID is reset to zero.

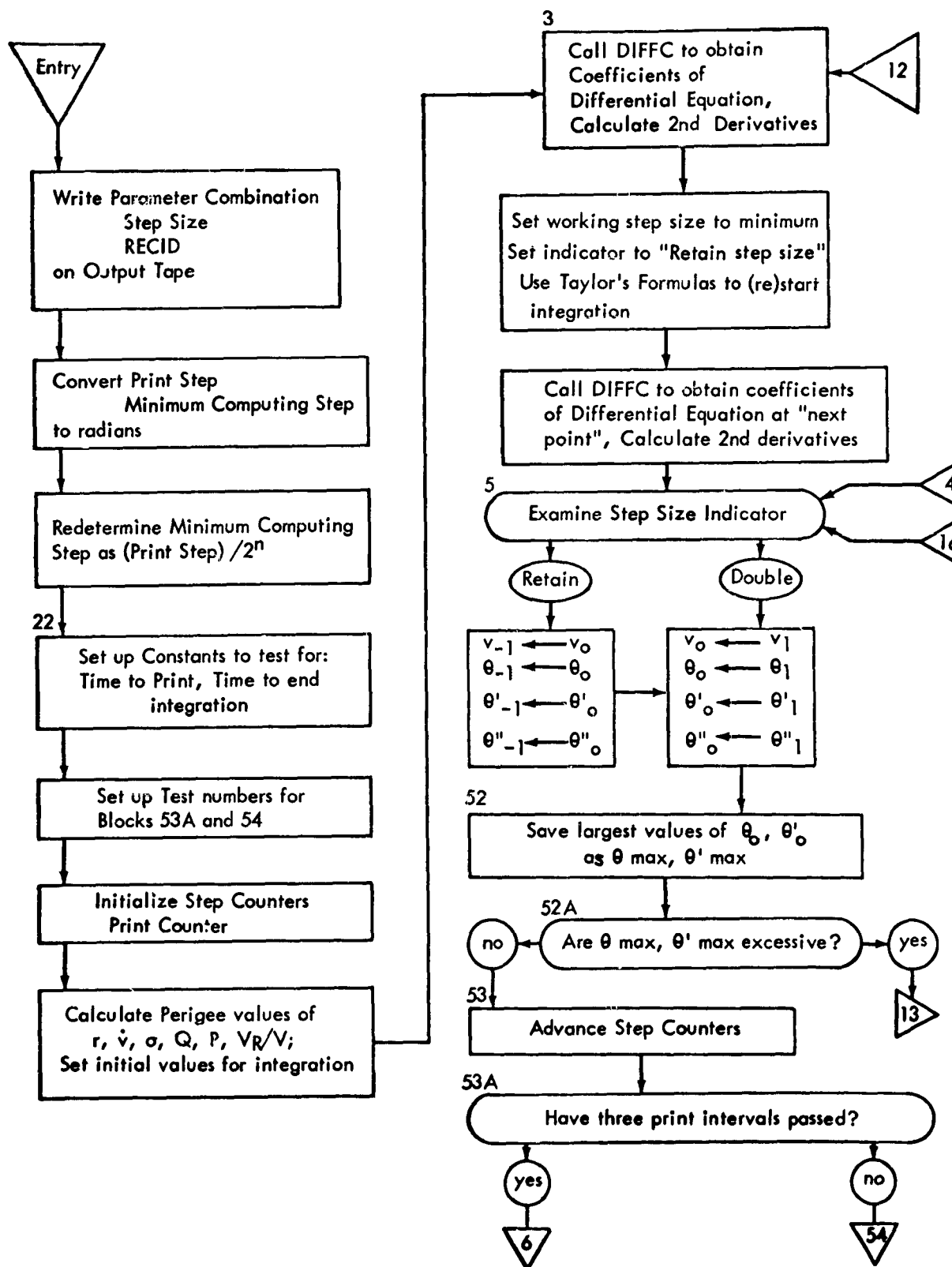
- d. Sample Input Data with resulting output follow the compiled listings of the components of this program.

Note: The program symbol for v is PHI, for $\det(I-W)$ is DELTA.

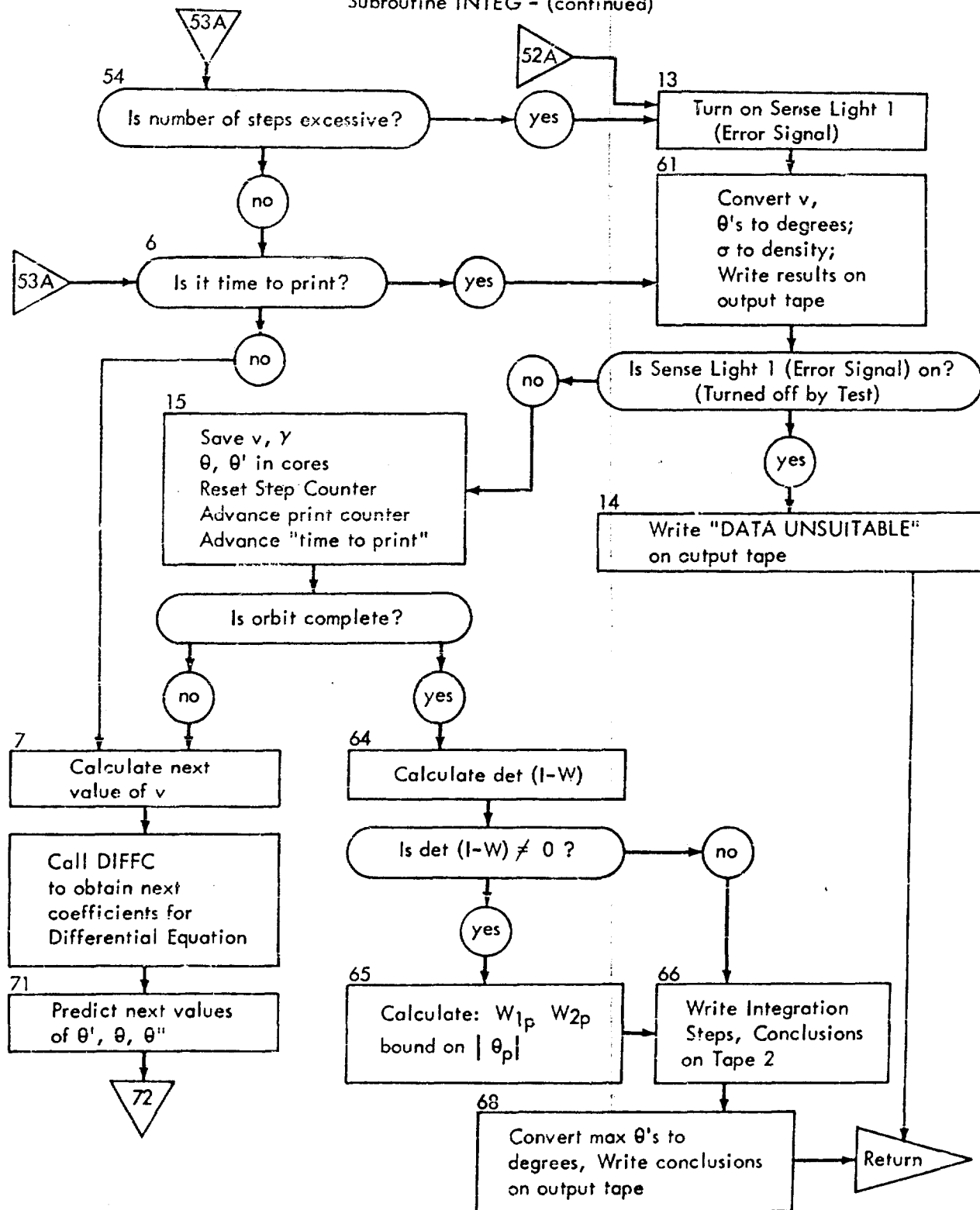
Main Program for Part I



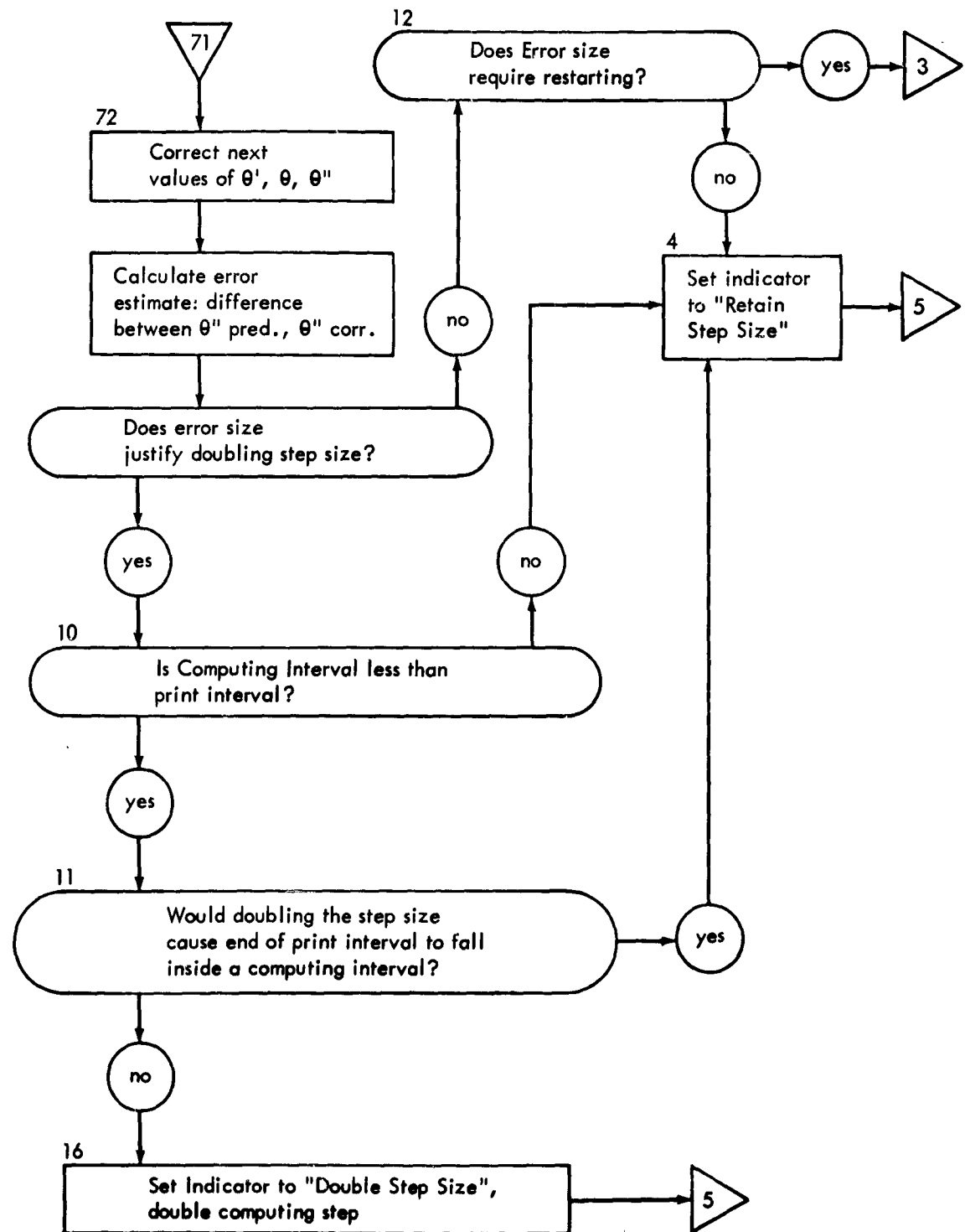
27
Subroutine INTEG



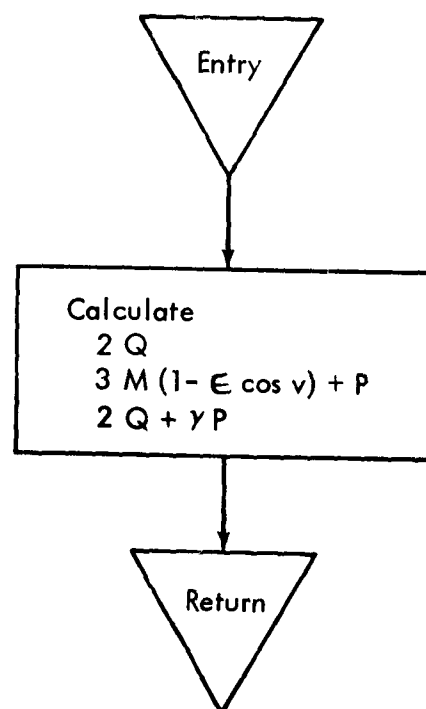
Subroutine INTEG - (continued)



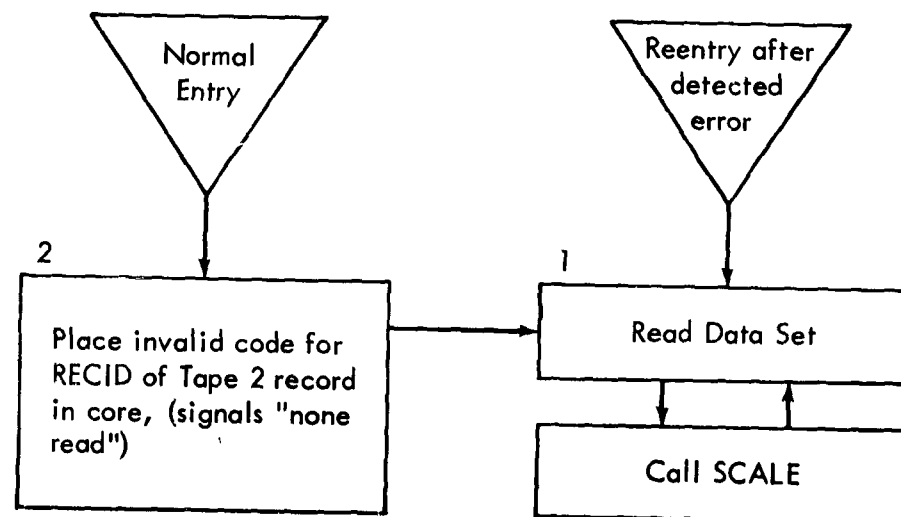
Subroutine INTEG - (concluded)



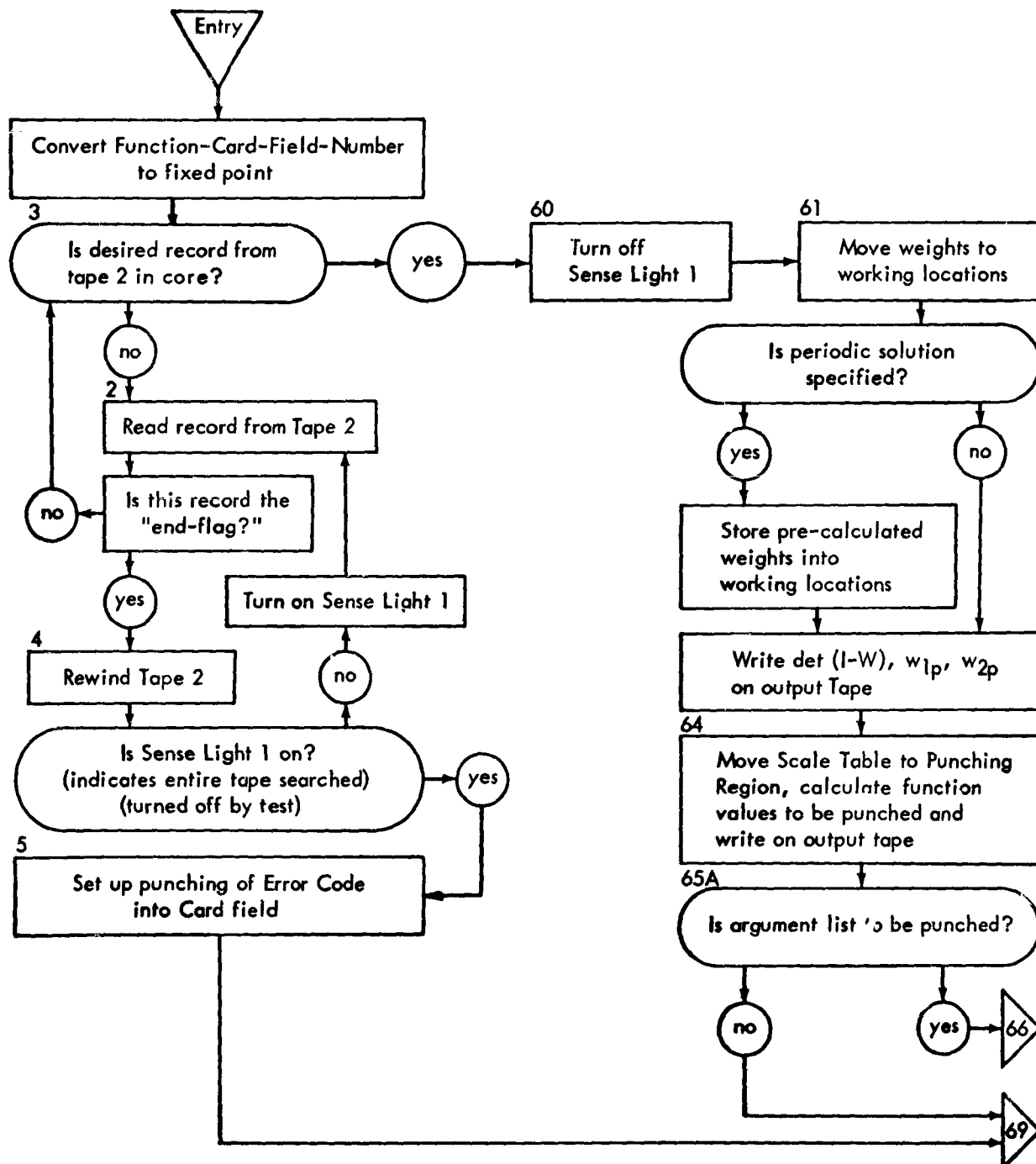
Subroutine DIFFC



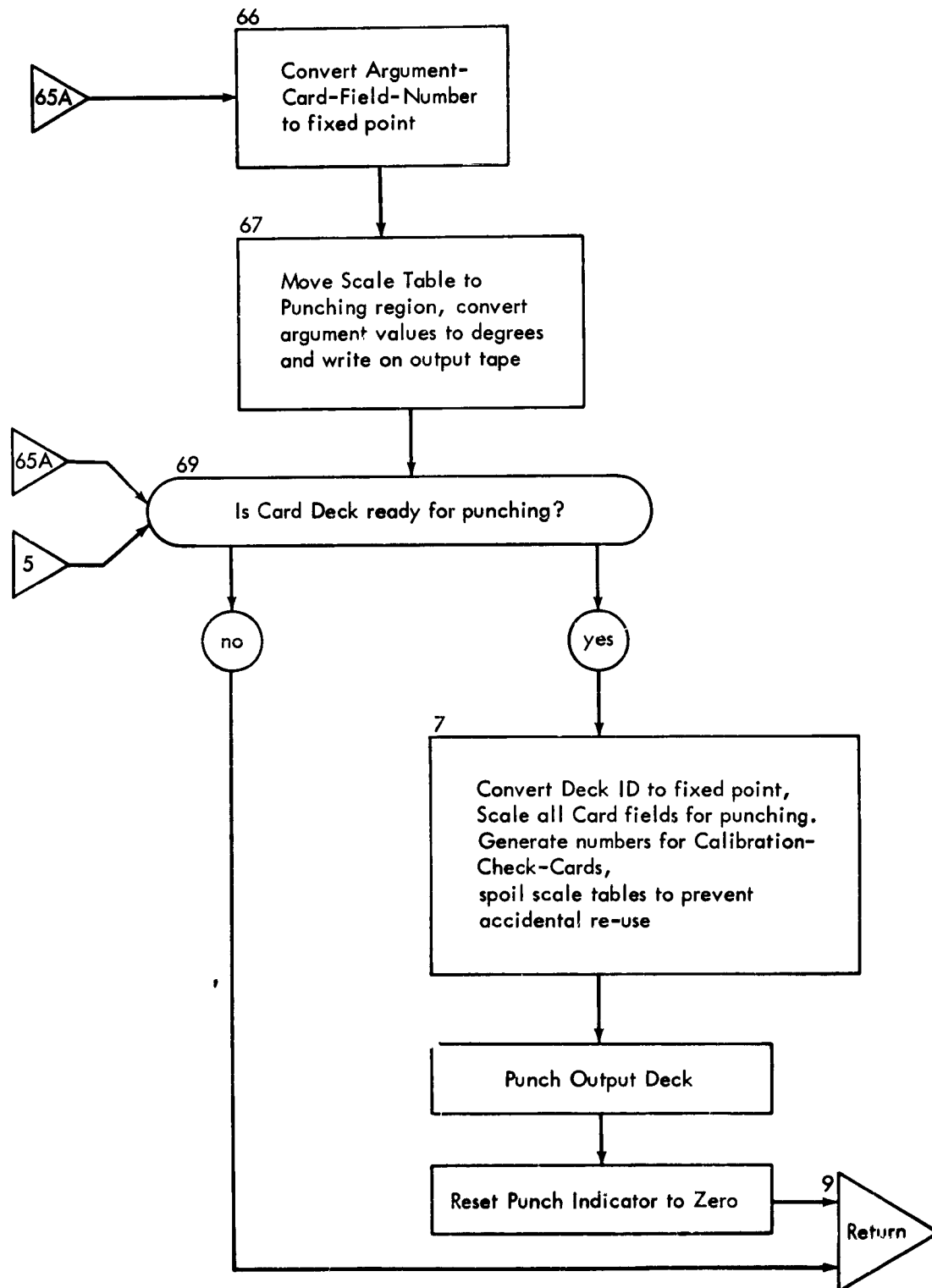
Main Program for Part II



Subroutine SCALE



Subroutine SCALE - (concluded)



C	MAIN PROGRAM TO VARY THROUGH LISTS OF VARIABLES	1M091300
	DIMENSION C(260),D(260)	1M091302
	COMMON C	1M091304
	EQUIVALENCE (C,D)	1M091306
	IF DIVIDE CHECK 1,4	1M091307
4	REWIND 2	1M091308
	YD=-1.	1M091309
	NS=1	1M091310
1	CALL FXRCH(D)	1M091312
	IF (C(28)) 6,5,2	1M091314
2	CONTINUE	1M091316
	IM=D(201)	1M091318
	JM=D(211)	1M091320
	KM=D(221)	1M091322
	LM=D(231)	1M091324
	MM=D(241)	1M091326
	NM=D(251)	1M091328
	WRITE OUTPUT TAPE 6,11,(D(I+201),I=1,IM)	1M091330
	WRITE OUTPUT TAPE 6,12,(D(I+211),I=1,JM)	1M091332
	WRITE OUTPUT TAPE 6,13,(D(I+221),I=1,KM)	1M091334
	WRITE OUTPUT TAPE 6,14,(D(I+231),I=1,LM)	1M091336
	WRITE OUTPUT TAPE 6,15,(D(I+241),I=1,MM)	1M091338
	WRITE OUTPUT TAPE 6,16,(D(I+251),I=1,NM)	1M091340
	DO 3 I=1,IM	1M091342
	DO 3 J=1,JM	1M091344
	DO 3 K=1,KM	1M091346
	DO 3 L=1,LM	1M091348
	DO 3 M=1,MM	1M091350
	DO 3 N=1,NM	1M091352
	C(1)=D(I+201)	1M091354
	C(2)=D(J+211)	1M091356
	C(3)=D(K+221)	1M091358
	C(4)=D(L+231)	1M091360
	C(5)=D(M+241)	1M091362
	C(6)=D(N+251)	1M091364
	CALL INTEG	1M091366
	C(28)=C(28)+1.	1M091367
3	CONTINUE	1M091368
	GO TO 1	1M091370
11	FORMAT (18H1 PARAMETER LIST -/7H0 OI =(9F10.2))	1M091372
12	FORMAT (7H0 HP =(9F10.0))	1M091374
13	FORMAT (7H0 EC =(9F10.6))	1M091376

14	FORMAT (7H0 GAM =(9F10.3))	1M091378
15	FORMAT (7H0 GAMQ =(9F10.3))	1M091380
16	FORMAT (7H0 OM =(9F10.6))	1M091382
5	WRITE TAPE 2,YD,NS,(C(I),I=1,15)	1M091384
	END FILE 2	1M091386
	REWIND 2	1M091388
	GO TO 1	1M091390
6	C(8)=CHAINF(1,7)	1M091392
	STOP	1M091394
	END(0,0,0,0,0)	

STORAGE FOR VARIABLES APPEARING IN COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
D	32562	77462	C	32562	77462		

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
4	5	00012	4	5	00012	1	8	00017
2	11	00027	3	68	00343	11	70	00000
13	72	00000	14	73	00000	15	74	00000
5	76	00366	5	82	00400	6	86	00405

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
317	00475	32302	77056

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
INTEG	2 00002	FXRCH	7 00007	CHAIN	0 00000	(FIL)	3 00003
(IOH)O	5 00005	(LEV)	6 00006	(RTN)	1 00001	(STH)	4 00004

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION-EQUIVALENCE OR COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
IM	316 00474	JM	315 00473	KM	314 00472	LM	313 00471
MM	312 00470	NM	311 00467	NS	310 00466	YD	309 00465

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
E110K	198 00306	E110J	191 00277	D120L	203 00313	D120K	199 00307
D120J	192 00300	D120I	185 00271	C1G5	308 00464	C1G4	307 00463
C1G3	306 00462	C1G2	305 00461	C1G1	304 00460	81G	280 00430
81F	284 00434	81E	288 00440	81D	292 00444	81C	296 00450
81B	303 00457	21	269 00415	31	271 00417	61	272 00420

SUBROUTINES NOT PUNCHED FROM LIBRARY

FXRCH	(LEV)	(IOH)O	(STH)	(FIL)	INTEG	(RTN)	CHAIN
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SUBROUTINE INTEG
  PREDF(YL,YO,YPL,YPO)=YL+4.*(YL-YO+DPC*(YPL+YPO
2 +YPO)/2.)
  SIMPF(YL,YPL,YPO,YPN)=YL+DPC*(YPL+4.*YPO+YPN)/3.
  RELERF(A,B)=ABSF(A-B)/MAX1F(ABSF(A),ABSF(B),1.E-7)
  DIMENSION C(200),VMAX(2,3),PHI(3),V(3,4,3),CO(3),
2 SAV(2,4,360),PRBL(8)
  COMMON C
  EQUIVALENCE (C(32),TBL(1),SIG(14),R(15),H(16),QP(17),
2 PP(18),VRVV(19),SIGP(20),THPC(21),THO(22),PHIO(23),
3 EC(30),HP(31),OI(32),PHMAX(5),OM(27),GAMQ(28),GAM(29))
4 ,(GAMMA(4),RE(3),OMU(2),C(32)),(N,PRBL(8))
  WRITE OUTPUT TAPE 6,1,(C(I),I=1,7),C(9),C(28)
  FORMAT (1H18X2H0113X2HHP13X2HEC13X3HGAM11X4HGAMQ12X
2 2HOM/F13.2,F15.0,F15.0,1P17.4,E15.4,0PF13.6/1H0
3 4X9HD PHI MIN5X11HD PHI PRINT51X9HRECORD ID/
4 1P2E15.4,0PF60.0/1H08X3HPH112X1HH7X3HRH016X5HGAMMA
5 6X8HALPHA H16X8HALPHA H2 6X8ALPHA PA6X1HN)
  DPPR=C(9)/57.295780
  DPLIM=C(7)/57.295780
  DPMIN=DPPR
  DPTST=DPMIN/2.
23 IF (DPMIN-DPLIM) 22,22,21
21 DPMIN=DPMIN/2.
  GO TO 23
22 PHPR=DPPR-DPTST
  PHEND=6.2831853-DPTST
  FNRA=DPPR/DPTST
  NRAT=FNRA
  N=0
  NT=0
  NS=1
  RP=HP+RE
  PHDP=SQRTF(OMU*(1.+EC)/RP)/RP
  CALL ATMOS (HP,TBL,R)
  SIGP=SIG
  QP=GAMQ*SIGP*RP*2.9711463E-4
  PP=GAM*SIGP*RP**2*1.1884585E-3
  VRVV=1.-7.292 1151E-5*COSF(OI/57.295780)/PHDP
  PHI(2)=0.
  V(1,2,1)=1.7453293E-2
  VMAX(1,1)=1.7453293E-2

```

1M091416
1M091418
1M091420
1M091422
1M091424
1M091426
1M091427
1M091428
1M091430
1M091432
1M091434
1M091436
1M091438
1M091440
1M091442
1M091444
1M091446
1M091448
1M091450
1M091452
1M091454
1M091456
1M091458
1M091460
1M091462
1M091464
1M091466
1M091468
1M091470
1M091472
1M091474
1M091476
1M091478
1M091480
1M091482
1M091484
1M091486
1M091488
1M091490
1M091492
1M091494
1M091496

```

V(1,2,2)=0.
VMAX(1,2)=0.
V(1,2,3)=0.
VMAX(1,3)=0.
V(2,2,1)=0.
VMAX(2,1)=0.
V(2,2,2)=1.
VMAX(2,2)=1.
V(2,2,3)=0.
VMAX(2,3)=0.
CALL DIFFC(PHI(2),CO)
DO 31 I=1,3
  V(3,2,1)=-V(2,2,1)*CO(1)-V(1,2,I)*CO(2)
  V(3,2,3)=V(3,2,3)+CO(3)
DPC=DPMIN
M=1
PHI(3)=PHI(2)+DPC
CALL DIFFC(PHI(3),CO)
DO 32 I=1,3
  V(1,3,I)=V(1,2,I)+DPMIN*(V(2,2,I)+DPMIN*V(3,2,I)/2.)
  V(2,3,I)=V(2,2,I)+DPMIN*V(3,2,I)
  V(3,3,I)=-V(2,3,I)*CO(1)-V(1,2,I)*CO(2)
  V(3,3,3)=V(3,3,3)+CO(3)
DO 51 J=M,2
  PHI(J)=PHI(J+1)
DO 51 K=1,3
DO 51 I=1,3
  V(I,J,K)=V(I,J+1,K)
DO 52 J=1,3
DO 52 I=1,2
  VMAX(I,J)=MAX1F(VMAX(I,J),ABSF(V(I,2,J) ) )
  IF (MAX1F(VMAX(1,1),VMAX(1,2),VMAX(1,3) )-174532.93) 53,13,13
N=N+1
NT=NT+1
IF (PHI(2)-3.*DPPR) 54,6,6
IF (NT-NRAT) 6,6,13
IF (PHI(2)-PHPR) 7,61,61
PRBL(1)=57.295780*PHI(2)
PRBL(2)=H
PRBL(4)=57.295780*GAMMA
PRBL(3)=2.376 917E-3*SIG
DO 62 I=1,3

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1M091498
1M091500
1M091502
1M091504
1M091506
1M091508
1M091510
1M091512
1M091514
1M091516
1M091518
1M091520
1M091522
1M091524
1M091526
1M091528
1M091530
1M091532
1M091534
1M091536
1M091538
1M091540
1M091542
1M091544
1M091546
1M091548
1M091550
1M091552
1M091554
1M091556
1M091558
1M091560
1M091562
1M091564
1M091566
1M091568
1M091570
1M091572
1M091574
1M091576
1M091578
1M091580

```

62  PRBL(I+4)=57.295780*V(1,2,I)-FRBL(4)
    WRITE OUTPUT TAPE 6,2,(PRBL(I),I=1,8)
    FORMAT (F14.3,F14.0,1PE14.4,OP4F14.3,17)
14  IF (SENSELIGHT 1) 14,15
17  WRITE OUTPUT TAPE 6,17
    FORMAT (16HODATA UNSUITABLE)
    GO TO 9
15  SAV(1,1,NS)=PHI(2)
    SAV(2,1,NS)=GAMMA
    DO 63 J=1,3
    DO 63 I=1,2
63  SAV(I,J+1,NS)=V(1,2,J)
    N=0
    NS=NS+1
    PHPR=PHPR+DPPR
    IF (PHI(2)-PHEND) 7,7,64
64  PRBL(1)=(1.-57.295780*V(1,2,1))*V(2,2,2)
    2 -V(2,2,1)*V(1,2,2)/1.7453293E-2
    PRBL(2)=0.
    PRBL(3)=0.
    PRBL(4)=0.
    IF (ABSF(PRBL(1))-1.E-6) 66,66,65
65  PRBL(2)=57.295780*(V(1,2,3)*(1.-V(2,2,2))+V(2,2,3)
    2 *V(1,2,2))/PRBL(1)
    PRBL(3)=(1.-57.295780*V(1,2,1))*V(2,2,3)+V(2,2,1)
    2 *V(1,2,3)/1.7453293E-2)/PRBL(1)
    PRBL(4)=VMAX(1,3)+ABSF(PRBL(2))*VMAX(1,1)
    2 +ABSF(PRBL(3))*VMAX(1,2)
    DO 67 I=1,3
66  PRBL(I+4)=VMAX(1,I)
67  NS=8*NS-8
    C
    DIMENSION SAV1(2880)
    EQUIVALENCE (SAV1,SAV)
    C
    WRITE TAPE 2,C(28),NS8,(SAV1(I),I=1,NS8),(PRBL(I),I=1,7)
    DO 68 I=1,4
68  PRBL(I+3)=57.295780*PRBL(I+3)
    WRITE OUTPUT TAPE 6,1,(C(I),I=1,7),C(9)
    WRITE OUTPUT TAPE 6,69,C(28),FRBL(1),(V(2,2,I),I=1,3),
    2 NT,PRBL(4),PRBL(2),(PRBL(I+4),I=1,3),PRBL(3),(VMAX(2,I),I=1,3)
69  FORMAT (1H+F89.0/1H031X5HDELTA23X15HEND DERIVATIVES28X2HNT/

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1M091582

1M091584

1M091586

1M091588

1M091590

1M091592

1M091594

1M091596

1M091598

1M091600

1M091602

1M091604

1M091606

1M091608

1M091610

1M091612

1M091614

1M091616

1M091618

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1M091622

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1M091628

1M091630

1M091632

1M091634

1M091636

1M091638

1M091640

1M091642

1M091643

1M091644

1M091646

1M091647

1M091648

1M091650

1M091652

1M091654

1M091656

1M091658

1M091660


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2 1PE42.4,OP14X3F14.3,I7//20X27HTH PER BD  WEIGHT THETA H1
3 13X10HMAX THETAS/18X1P2E12.4,I4XOP3F14.3//32X
4 15HWEIGHT THETA H213X15HMAX DERIVATIVES/1PE42.4,14X
5 OP3F14.3)
9 RETURN
7 PHI(3)=PHI(2)+DPC
  CALL DIFFC(PHI(3),CO)
  DO 71 I=1,3
    V(2,4,I)=PREDF(V(2,1,I),V(2,2,I),V(3,1,I),V(3,2,I))
    V(1,4,I)=SIMPV(V(1,1,I),V(2,1,I),V(2,2,I),V(2,4,I))
    V(3,4,I)=-V(2,4,I)*CO(1)-V(1,4,I)*CO(2)
    V(3,4,3)=V(3,4,3)+CO(3)
  DO 72 I=1,3
    V(2,3,I)=SIMPV(V(2,1,I),V(3,1,I),V(3,2,I),V(3,4,I))
    V(1,3,I)=SIMPV(V(1,1,I),V(2,1,I),V(2,2,I),V(2,3,I))
    V(3,3,I)=-V(2,3,I)*CO(1)-V(1,3,I)*CO(2)
    V(3,3,3)=V(3,3,3)+CO(3)
  ERR=0.
  DO 73 I=1,3
    ERR=MAX1F(ERR,RELERF(V(3,4,I),V(3,3,I)))
    IF (ERR-1.E-6) 10,10,12
  IF (DPC+DPC-DPPR) 11,11,4
10 TEST=.5*(PHPR+DPTST-PHI(3))/DPC
11 IF (INTF((TEST-INTF(TEST+.5))*FNKRAT)) 4,16,4
16 M=2
  DPC=DPC+DPC
  GO TO 5
4 M=1
  GO TO 5
12 IF (ERR-1.E-4) 4,4,3
13 SENSELIGHT 1
  GO TO 61
  END(0,0,0,0,0)

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1M091662
1M091664
1M091666
1M091668
1M091670
1M091672
1M091674
1M091676
1M091678
1M091680
1M091682
1M091684
1M091686
1M091688
1M091690
1M091692
1M091694
1M091696
1M091698
1M091700
1M091702
1M091704
1M091706
1M091708
1M091710
1M091711
1M091712
1M091714
1M091716
1M091718
1M091720
1M091722

```

STORAGE FOR VARIABLES APPEARING IN COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
H 32546	77442	HP 32561	77461	GAM 32559	77457	GAMQ 32558	77456
GAMMA 32534	77426	EC 32560	77460	C 32562	77462	OI 32562	77462
OM 32557	77455	OMU 32532	77424	PHIO 32553	77451	PHMAX 32535	77427
PP 32548	77444	QP 32547	77443	RE 32533	77425	R 32545	77441
SIGP 32550	77446	SIG 32544	77440	TBL 32531	77423	THO 32552	77450
THPO 32551	77447	VRVV 32545	77445				

NAMES OF ARITHMETIC STATEMENT FUNCTIONS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

PRED	IFN	LOC	IFN	LOC	REL	IFN	LOC
	2	01517	SIMP	3	01533	4	01543

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
1	14	00000	23	18	00053	21	20	00063
3	50	00236	3	51	00236	31	53	00244
5	65	00330	51	65	00354	52	72	00377
54	77	00446	6	78	00452	61	79	00457
2	91	00000	14	92	00525	14	94	00534
15	97	00537	63	101	00557	64	106	00610
66	114	00714	67	115	00716	68	130	00753
9	153	01052	7	155	01056	71	161	01117
73	170	01205	10	172	01230	11	173	01235
4	178	01267	12	180	01272	13	181	01277

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
3854	07416	32362	77152

LOCATIONS OF NAMES IN TRANSFER VECTOR

DIFFC	DEC	OCT	DIFFC	DEC	OCT
(FIL)	1	00001	(IOH)O	2	00002
(STH)	5	00005	COS	7	00007
	6	00006	(IOH)O	8	00010
			ATMOS	3	00003
			(LEV)	8	00010
			SQRT	4	00004
			(RTN)	0	00000

DEC	OCT	DEC	OCT	DEC	OCT
CO	962 01702	N	3846 07406	PHI	965 01705
SAV1	3845 07405	SAV	3845 07405	VMAX	959 01677
				PRBL	3853 07415
				V	953 01677

	DEC	OCT	DEC	OCT	DEC	OCT
FNRAT	917	01625	ERR	916	01624	
DPMIN	913	01621	DPLIM	912	01620	
NRAT	909	01615	NS8	908	01614	
PHDP	905	01611	PHEND	904	01610	
TEST	901	01605				
			DPTST			DEC
			DPC			OCT
			NS			915
			PHPR			01623
						911
						01617
						907
						01613
						903
						01607
						DPPR
						M
						910
						01616
						NT
						906
						01612
						RP
						902
						01606

	DEC	OCT	DEC	OCT	DEC	OCT
EIM	281	00431	C11G4	90C	01604	DEC
81H	780	01414	812	786	01422	8125
81J	893	01575	21	705	01301	1)
6)	727	01327	71	888	01570	411
						DEC
						OCT
						8125
						776
						01410
						896
						01600
						889
						01571

(LEV) (RTN)	(IOH)O (STH)	SUBROUTINES NOT PUNCHED FROM LIBRARY (FIL)	SORT	ATMOS	COS	DIFFC
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SUBROUTINE DIFFC(PHI,V)
DIMENSION C(200),V(3)
COMMON C
EQUIVALENCE (C(32),TBL(1),SIG(14),R(15),H(16),QP(17),
2 PP(18),VRVV(19),SIGP(20),THPO(21),THQ(22),PHIO(23),
3 EC(30),HP(31),OI(32),PHMAX(5),OM(27),GAMQ(28),GAM(29))
4 ,(GAMMA(4),RE(3),OMU(2),C(32))
SINP=SINF(PHI)
COSP=COSF(PHI)
GAMMA=EC*SINP/(1.+EC*COSP)
EOMCP=EC*(1.-COSP)
RV=(HP+RE)*(1.+EC)/(1.+EC*COSP)
H=RV-RE
CALL ATMOS(H,TBL,R)
RRVV=SIG*VRVV/SIGP
TWOQ=QP*RRVV*(1.+EOMCP)-EC*SINP
V(1)=TWOQ+TWOQ
PTIL=PP*RRVV*VRVV*(1.+EOMCP+EOMCP)
V(2)=OM*(1.-EC*COSP)/.333 3333+PTIL
V(3)=GAMMA*PTIL+TWOQ+TWOQ
RETURN
END(0,0,0,0,0)

```

STORAGE FOR VARIABLES APPEARING IN COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
H 32546	77442	HP 32561	77461	GAM 32559	77457	GAMQ 32558	77456
GAMMA 32534	77426	EC 32560	77460	C 32562	77462	OI 32562	77462
OM 32557	77455	OMU 32532	77424	PHIO 32553	77451	PHMAX 32535	77427
PP 32548	77444	QP 32547	77443	RE 32533	77425	R 32545	77441
SIGP 32550	77446	SIG 32544	77440	TBL 32531	77423	THQ 32552	77450
THPO 32551	77447	VRVV 32549	77445				

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
133 00205		32362	77152

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT
COS	1 00001	ATMOS	0 00000	SIN	2 00002

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION-EQUIVALENCE OR COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT
EOMCP	132 00204	COSP	131 00203	PTIL	130 00202
RV	128 00200	SINP	127 00177	TWOQ	126 00176
				RRVV	129 00201

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT
9)	121 00171	1)	123 00173	3)	114 00162
7)	122 00172			6)	116 00164

SUBROUTINES NOT PUNCHED FROM LIBRARY

SIN	COS	ATMOS
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C      CHAIN(1) PROGRAM TO SCALE FOR PUNCHING
      DIMENSION C(20)
      COMMON C
      IF DIVIDE CHECK 1,2
      C(20)=0.
      CALL FXRCH(C)
      CALL SCALE
      GO TO 1
      END(0,0,0,0,0)

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```

1M091800
1M091801
1M091802
1M091803
1M091804
1M091805
1M091806
1M091807

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STORAGE FOR VARIABLES APPEARING IN COMMON SENTENCES

DEC OCT
C 32562 77462

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
2	4	00004	1	5	00006	1	6	00006

STORAGE NOT USED BY PROGRAM

DEC OCT
20 00024

DEC OCT
32542 77436

LOCATIONS OF NAMES IN TRANSFER VECTOR

46

FXRCH	DEC	OCT	SCALE	DEC	OCT	DEC	OCT
	1	00001	0	00000			

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

3)	DEC	OCT	DEC	OCT	DEC	OCT
	14	00016	6)	15	00017	

SUBROUTINES NOT PUNCHED FROM LIBRARY

FXRCH SCALE

	SUBROUTINE SCALE	1M091820
	DIMENSION C(20), SAV(8,120), SAV1(960), PNCH(121,16), IPNCH(121,16),	1M091822
	2 SPNCH(5,16), PRBL(7), ISPNCH(5,16)	1M091824
	COMMON C	1M091826
	EQUIVALENCE (SAV, SAV1), (PNCH, IPNCH), (SPNCH, ISPNCH)	1M091827
	WRITE OUTPUT TAPE 6,1,(C(I),I=1,18)	1M091828
1	FORMAT (1H16X11HTAPE RECORD5X26HWEIGHT PAR WEIGHT GAMMA	1M091830
	2 4X9HWEIGHT HI6X9HWEIGHT H2/F18.0,1PE16.6,3E15.6/	1M091832
	3 33HOSCALING ~ MIN VALUE MIN COUNTS5X9HMAX VALUE6X	1M091834
	4 39HMAX COUNTS EDGE COUNTS CARD FIELD/	1M091836
	5 9H FUNCTIONOPF11.3,F13.0,F14.3,F16.0,F15.0,F14.0/	1M091838
	6 9H ARGUMENT F11.3,F13.0,F14.3,F16.0,F15.0,F14.0/	1M091840
	7 10HODECK ID -F7.0)	1M091842
	J=C(11)+.5	1M091844
3	IF (INTF(C(20)+.5)-INTF(C(1)+.5)) 2,60,2	1M091846
2	READ TAPE 2,C(20),NS8,(SAV1(I),I=1,NS8),(PRBL(I),I=1,7)	1M091848
4	IF (C(20)) 4,3,3	1M091850
	REWIND 2	1M091852
5	IF (SENSELIGHT 1) 5,6	1M091854
	SPNCH(1,J)=SPNCH(3,J)	1M091856
6	GO TO 69	1M091858
	SENSELIGHT 1	1M091860
	GO TO 2	1M091862
60	IF (SENSELIGHT 1) 61,61	1M091864
61	WH1=C(4)	1M091866
	WH2=C(5)	1M091868
	WP=ABSF(C(2))	1M091870
	IF (C(2)) 62,63,63	1M091872
62	WH1=PRBL(2)	1M091874
	WH2=PRBL(3)	1M091876
63	NS=NS8/8	1M091878
	CALL WRITE(6HOD WHS,PRBL,3)	1M091879
	DO 64 I=1,5	1M091880
64	SPNCH(I,J)=C(I+5)	1M091882
	PNCH(1,J)=WH1	1M091884
	DO 65 I=1,NS	1M091886
65	PNCH(I+1,J)=(C(3)*SAV(2,I)+WP*SAV(7,I)+WH1*SAV(3,I)	1M091888
	2 +WH2*SAV(5,I))*57.295780	1M091890
	N=NS+1	1M091892
	CALL WRITE(6HOFUNCTN,PNCH(1,J),N)	1M091894
	IF (C(17)) 69,69,66	1M091896
66	J=C(17)+.5	1M091898

67	DO 67 I=1,5 SPNCH(I,J)=C(I+11) PNCH(1,J)=0. DO 68 I=1,NS PNCH(I+1,J)=57.295780*SAV(1,I) CALL WRITE (6H0 ARG,PNCH(1,J),N) 69 IF (C(18)) 9,9,7 7 ID=C(18)+.5 DO 72 J=1,16 ISPCH(5,J)=SPNCH(5,J) DO 71 I=1,N IPNCH(I,J)=XMINOF(ISPNCH(5,J),NP SCL(PNCH(I,J),SPNCH(1,J))) 71 SPNCH(3,J)=SPNCH(1,J) 72 ISPNCH(4,J)=0 N1=N+1 N2=N1+1 PUNCH 73,(ID,I,(IPNCH(I,J),J=1,16),I=1,N),ID,N1, 2 (ISPNCH(4,J),J=1,16),ID,N2,(ISPNCH(5,J),J=1,16) 73 FORMAT (1H013,17I4) PUNCH 74,ID 74 FORMAT (1H-13/1H) C(18)=0. 9 RETURN END(0,0,0,0,0)	1M091900 1M091902 1M091904 1M091906 1M091908 1M091910 1M091912 1M091914 1M091916 1M091918 1M091920 1M091922 1M091923 1M091924 1M091926 1M091928 1M091930 1M091932 1M091934 1M091936 1M091938 1M091940 1M091942
----	-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------

STORAGE FOR VARIABLES APPEARING IN COMMON SENTENCES

	DEC	OCT	DEC	OCT	DEC	OCT
C	32562	77462				

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
1	11	00000	3	13	00053	2	14	00066
4	25	00116	4	25	00116	5	27	00122
60	31	00127	61	32	00131	62	36	00143
64	42	00175	65	45	00222	66	50	00270
68	55	00343	69	58	00363	7	59	00367
71	64	00432	72	66	00455	73	85	00000
9	91	00574				74	89	00000

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
3498	06652	32542	77436

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT
NPSCL	1 00001	WRITE	2 00002	(FIL)	4 00004
(LEV)	7 00007	(RTN)	3 00003	(SCH)	0 00000
				(STH)	5 00005

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT
ISPNCN	601 01131	IPNCN	2537 04751	PNCH	2537 04751
SAV1	3497 06651	SAV	3497 06651	SPNCH	601 01131

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION,EQUIVALENCE OR COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT
I	514 01002	ID	513 01001	J	512 01000
N2	510 00776	N	509 00775	NS8	508 00774
WH1	506 00772	WH2	505 00771	WP	504 00770

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT

	DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
E117	379	00573	D110A	81	00121	C1102	503	00767
B1	491	00753	A1102	482	00742	A1100	473	00731
8129	403	00623	811	472	00730	11	497	00761
31	390	00606	61	393	00611			

	DEC	OCT
	502	00766
	400	00620
	384	00600

(LEV)	(IOH)O	(STH)	(FIL)	(RTN)	WRITE	NPSCL	(SCH)
SUBROUTINES NOT PUNCHED FROM LIBRARY							

APPENDIX B

PROGRAM DESCRIPTION - ATMOSPHERE SUBROUTINE
NORTH AMERICAN AVIATION, INC. COLUMBUS
ENGINEERING PROGRAM DESCRIPTION

1. Identification

- a. Atmosphere Subroutine, 1F113
- b. Sarah Crooke, August 1959
- c. Aero Advanced Design Group - 214
- d. Fortran Source Deck is up to date.

2. Purpose

Calculates standard atmosphere properties at a specified altitude.

3. Restrictions

Fortran 2 subroutine subprogram.

4. Method

Table look-up of properties at base geopotentials followed by application of the ideal gas law.

5. Use

Subroutine is reached by Fortran Statement

CALL ATMOS (H, TBL, R)

where H is the input altitude

TBL is the table of base geopotentials and properties

R is the results array.

6. Coding Information

- a. This routine occupies 309 Locations.
- b. Inferior Subroutines are Library routines DUMP, EXP, SQRT, and the Fortran system routine EXP(3).

7. Data Arrangement

- a. The array TBL must contain the following data:

<u>Location</u>	<u>Description</u>	<u>Symbol</u>
1	Sea Level Temperature, °R	T ₀
2	Sea Level Pressure, lb/ft ²	P ₀

<u>Location</u>	<u>Description</u>	<u>Symbol</u>
3	Sea Level Gas Constant, $\text{ft}^2/\text{sec}^{20}\text{R}$	R_o
4	Sea Level Density, slugs/ft^3	ρ_o
5	Number of Base Geopotentials in Table	n
6	Base Geopotentials, ft	h_o
\vdots		
$5 + n$		
$6 + n$		
\vdots	Base Gas Constants, $\text{ft}^2/\text{sec}^{20}\text{R}$	R_o
$5 + 2n$		
$6 + 2n$		
\vdots	Base Temperatures, $^{\circ}\text{R}$	T_o
$5 + 3n$		
$6 + 3n$		
\vdots	Base Specific Heat Ratios, dimensionless	γ_o
$5 + 4n$		
$6 + 4n$		
$7 + 4n$	$A_i \times 10^6$ is the i th Base Pressure Ratio, dimensionless	δ_o
\vdots		
$4 + 6n$		
$5 + 6n$		

b. On return the array R will contain the following data:

<u>Location</u>	<u>Description</u>	<u>Symbol</u>
1	Geopotential Altitude, ft	h
2	Density Ratio, dimensionless	σ
3	Speed of Sound, ft/sec	a
4	Speed of Sound, knots	A
5	Pressure Ratio, dimensionless	δ
6	Local Acceleration of Gravity, ft/sec^2	g

<u>Location</u>	<u>Description</u>	<u>Symbol</u>
7	Temperature, °R	T
8	Gas Constant, ft ² /sec ² °R	R
9	Incompressible Dynamic Pressure at Mach 1, lb/ft ²	G
10	Ratio of Specific Heats, dimensionless	γ

8. Formulas

In the formulas below H is the input altitude. The remaining symbols are those listed in 7 above. The subscript θ refers to the value of the quantity at the i th base geopotential altitude, where

$$i = 1 \text{ if } h < h_2,$$

$$i = j \text{ if } h_j \leq h < h_{j+1}, \quad j = 2, \dots, n-1,$$

$$i = n-1 \text{ if } h_n \leq h.$$

The prefix Δ denotes the increment of the quantity from the i th to the $(i+1)$ th base geopotential altitude.

$$h = \frac{20891000H}{H + 20891000}$$

$$T = T_\theta + (h - h_\theta) \frac{\Delta T}{\Delta h}$$

$$R = R_\theta + (h - h_\theta) \frac{\Delta R}{\Delta h}$$

$$\delta = \delta_\theta \left[\frac{R_\theta}{R} \frac{T}{T_\theta} \right]^{32.174049 \Delta h / (T_\theta \Delta R - R_\theta \Delta T)},$$

$$\text{if } T_\theta \Delta R - R_\theta \Delta T \neq 0$$

$$= \delta_\theta e^{-32.174049 (h - h_\theta) / \Delta h},$$

$$\text{if } T_\theta \Delta R - R_\theta \Delta T = 0$$

$$\sigma = \delta \frac{T_o}{T} \frac{R_o}{R}$$

$$\gamma = \gamma_o + (h - h_o) \frac{\Delta \gamma}{\Delta h}$$

$$g = 32.174049 \left[\frac{20\,891\,000}{H + 20\,891\,000} \right]^2$$

$$a = \sqrt{\frac{\gamma P_o \delta}{\rho_o \sigma}}$$

$$A = \frac{a}{1.6878099}$$

$$G = \frac{1}{2} (\rho_o \sigma) a^2$$

```

SUBROUTINE ATMOS(H, TABLE, RES)
  DIMENSION TABLE(100), RES(10), R(10)
  R(1) = H * 20891000. / (H + 20891000.)
  I = TABLE(5)
  IF (I - 1) 5, 5, 10
  R(1) = DUMPF(1)
  DO 20 K = 2, I
    IF (TABLE(K + 5) - R(1)) 20, 15, 15
  20 CONTINUE
  K = I
  HB = TABLE(K + 4)
  R(3) = TABLE(K + 5) - HB
  J = I + K
  RB = TABLE(J + 4)
  DRDH = (TABLE(J + 5) - RB) / R(3)
  J = J + I
  TB = TABLE(J + 4)
  DTDH = (TABLE(J + 5) - TB) / R(3)
  J = J + I
  GAMB = TABLE(J + 4)
  DGDH = (TABLE(J + 5) - GAMB) / R(3)
  J = J + I + K
  PBPO = TABLE(J + 2) * 10. ** TABLE(J + 3)
  R(9) = R(1) - HB
  R(7) = TB + DTDH * R(9)
  R(8) = RB + DRDH * R(9)
  R(10) = TB * DRDH - RB * DTDH
  IF (R(10)) 30, 25, 30
  R(2) = EXPF(-32.174049 * R(9) / (R(7) * R(8)))
  25 GOTO 35
  R(2) = (RB * R(7) / (R(8) * TB)) ** (32.174049 / R(10))
  30 R(5) = R(2) * PBPO
  35 R(2) = R(5) * TABLE(1) * TABLE(3) / (R(7) * R(8))
  R(10) = GAMB + DGDH * R(9)
  R(6) = 32.174049 * (20891000. / (20891000. + H)) ** 2
  R(3) = SQRTF(R(10) * R(5) * TABLE(2) / (TABLE(4) * R(2)))
  R(4) = R(3) / 1.6878099
  R(9) = .5 * R(3) * R(3) * TABLE(4) * R(2)
  DO 40 I = 1, 10
    RES(I) = R(I)
  40 RETURN
  END(0, 0, 0, 0, 0)

```

```

1F040100
1F040105
1F040110
1F040115
1F040120
1F040125
1F040130
1F040135
1F040140
1F040145
1F040150
1F040155
1F040160
1F040165
1F040170
1F040175
1F040180
1F040185
1F040190
1F040195
1F040200
1F040205
1F040210
1F040215
1F040220
1F040225
1F040230
1F040235
1F040240
1F040245
1F040250
1F040255
1F040260
1F040265
1F040270
1F040275
1F040280
1F040285
1F040290
1F040295
1F040300

```


EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
5	6	00106	10	7	00113	20	9	00132	15	11	00141
25	29	00254	30	31	00272	35	32	00312	40	40	00401

STORAGE NOT USED BY PROGRAM

DEC OCT
309 00465

LOCATIONS OF NAMES IN TRANSFER VECTOR

```

EXP(3      DEC      OCT
          2 00002
EXP      DEC      OCT
          1 00001
          DUMP      DEC      OCT
          SQRTR      DEC      OCT
          0 00000

```

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE SENTENCES

	DEC	OCT	DEC	OCT	DEC	OCT
R	308	00464				

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION•EQUIVALENCE OR COMMON SENTENCES

	DEC	OCT		DEC	OCT		DEC	OCT
I	298	00452	HB	297	00451	GAMB	296	00450
DRDH	294	00446	DGDH	293	00445	J	292	00444
PBPO	290	00442	RB	289	00441	TB	288	00440

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC		OCT		DEC		OCT		DEC		OCT		
E19	170	00252	E15	86	00126	C1G2	287	00437	DEC	286	00436	
9)	277	00425	1)	283	00433	2)	265	00411	C1G1	3)	267	00413
6)	272	00420	7)	282	00432							

```

DUMP      EXP(3      EXP      SUBROUTINES NOT PUNCHED FROM LIBRARY
                                SQRT

```

APPENDIX C

PROGRAM DESCRIPTION - FIXED DECIMAL CARD READ
ROUTINE WITH ERROR DETECTION
NORTH AMERICAN AVIATION, INC. COLUMBUS
ENGINEERING PROGRAM DESCRIPTION

1. Identification

- a. Fixed Decimal Card Read Routine with Error Detection - Deck NCF-FXRCH
- b. O. C. Juelich, March 1960
- c. Aero Advanced Design Group - 214
- d. Fortran Source Deck is up to date.

2. Purpose

- a. Load Input Data for Fortran II programs.
- b. Permit resumption of loading after cards with zero or fractional origin are found.
- c. List such error cards in the print-out.

3. Restrictions

- a. Reads input tape 5, writes output tape 6 in case of error.
- b. Data cards are written on Form 114-C-17 (Fortran Fixed 10 Digit Decimal Data).
- c. Uses Fortran II Error Procedure.

4. Method

- a. Card images are read from the input tape. The first word specifies the location to which the data is to be transmitted, and whether the data set is complete.
- b. Filled-in card fields are transmitted to the calling program, blank fields are not transmitted.
- c. Error Card images are written on the output tape. If error cards are found the error procedure is invoked at the end of the data set.

5. Use

- a. Subroutine is reached by the Fortran Statement:

CALL FXRCH (D) .

- b. A card image is read. The first word on the card is the subscript n , written with decimal point. The $(i+2)$ th word on the card; $i = 0, 1, 2, 3, 4$; is transmitted to location $D(|n|+i)$ as a floating point number unless it is blank or -0. If the $(i+2)$ th word is blank or -0 location $D(|n|+i)$ is unmodified. If n is positive this procedure is repeated. If n is negative control returns to the calling program. (Subscripting as in EQUIVALENCE statements.)

6. Coding Information

- a. This routine requires 17⁴ locations.
- b. Inferior subroutines are the Library routine ERRØR and Fortran System Subroutines.

C	FIXED DECIMAL CARD READ ROUTINE WITH ERROR DETECTION	
	SUBROUTINE FXRCH(D)	1F126000
	DIMENSION A(2),C(6),D(6)	1F126010
	I=1	1F126020
	1 READ INPUT TAPE 5,101,(C(J),J=1,6),A(1),A(2)	1F126030
	J=ABSF(C(1))	1F126040
4	IF (J) 2,99,2	1F126050
2	IF (C(1))-INTF(C(1)) 99,3,99	1F126060
3	DO 13 K=2,6	1F126070
	IF (C(K)) 12,11,12	1F126080
11	IF (SIGNF(1,C(K))) 13,13,12	1F126090
12	D(J)=C(K)	1F126100
13	J=J+1	1F126110
14	IF (SIGNF(1,C(1))) 20,20,1	1F126120
20	GO TO (40,30),I	1F126130
30	CALL ERROR	1F126140
40	RETURN	1F126150
99	GO TO (97,98),I	1F126160
97	I=2	1F126170
	WRITE OUTPUT TAPE 6,102	1F126180
98	WRITE OUTPUT TAPE 6,103,(C(J),J=1,6),A(1),A(2)	1F126190
	GO TO 14	1F126200
101	FORMAT (6F12.0,A6,A2)	1F126210
102	FORMAT (10H1BAD CARDS)	1F126220
103	FORMAT (F16.8,5E16.8,A6,A2)	1F126230
	FREQUENCY 4(0,0,1),2(0,1,0),11(1,0,1),14(1,0,5),20(1,0),	1F126240
	2 99(1,0)	1F126245
	END(0,0,0,0,0)	1F126248

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
1	4	00027	1	9	00050	4	11	00063
3	13	00075	11	15	00104	12	16	00112
14	18	00126	20	19	00134	30	20	00140
99	23	00151	97	24	00153	98	27	00172
101	34	00000	102	35	00000	103	36	00000

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
174	00256	32562	77462

LOCATIONS OF NAMES IN TRANSFER VECTOR

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
ERROR	3 00003	(FIL)	0 00000	(IOH)I	6 00006	(IOH)O	2 00002
(LEV)	7 00007	(RTN)	4 00004	(STH)	1 00001	(TSH)	5 00005

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT
C	171 00253	A	173 00255		

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION, EQUIVALENCE OR COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT
I	165 00245	J	164 00244		

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
E)H	121 00171	E)F	103 00147	E)D	95 00137	E)7	66 00102
D)409	77 00115	D)401	22 00026	D)20F	104 00150	D)20C	91 00133
D)108	85 00125	C)G3	163 00243	C)G2	162 00242	C)G0	161 00241
9)	160 00240	8)37	153 00231	8)36	156 00234	8)35	159 00237
2)	142 00216	3)	144 00220	6)	145 00221		

SUBROUTINES NOT PUNCHED FROM LIBRARY

(LEV)	(IOH)I	(TSH)	ERROR	(IOH)O	(STH)	(FIL)
-------	--------	-------	-------	--------	-------	-------

APPENDIX D

PROGRAM DESCRIPTION - PUNCH SCALING FUNCTION
NORTH AMERICAN AVIATION, INC. COLUMBUS
ENGINEERING PROGRAM DESCRIPTION

1. Identification

- a. Punch Scaling Function, Deck - NCF NPSCL.
- b. J. B. Burnett, May 1960.
- c. Digital Computing Group - 331.
- d. Source Deck is up to date.

2. Purpose

Converts floating point data to fixed point data which is scaled suitably for automatic plotting equipment.

3. Restrictions

Operates as a Fortran II Function Subprogram.

4. Method

Linear Scaling.

5. Use

- a. Reached through a Fortran Statement such as

IPNCH = NPSCL (A, S)

where A is the number to be scaled

S is an array of dimension 4 containing the scale table.

S(2) holds the plotter counts corresponding to the left or bottom edge of the graph

S(4) holds the plotter counts corresponding to the right or top edge of the graph

S(1) holds the value of A corresponding to S(2)

S(3) holds the value of A corresponding to S(4)

- b. S(2) and S(4) must be between 0.0 and 999.0, S(3) must exceed S(1). If the array S does not meet these specifications IPNCH will be set to -0.
- c. If A is less than S(1), IPNCH will be set to 0. If A exceeds S(3) IPNCH will be set to 999. (The user must make provision to confine the plotting head to the plotting bed.)

- d. It is expected that the plotting machine be set to 20 counts per centimeter, with (0, 0) counts at the lower left hand corner of the grid.

6. Coding Information

- a. This routine occupies 119 locations.
- b. There are no inferior subroutines.

	FUNCTION NPSC(LA,S)	NPSC(L300)
	DIMENSION S(4)	NPSC(L305)
	IF (S(3)-S(1)) 98,98,1	NPSC(L310)
1	DEN=S(3)-S(1)	NPSC(L315)
	IF (S(4)) 98,2,2	NPSC(L320)
2	IF (S(2)) 98,3,3	NPSC(L325)
3	IF (S(4)-999) 14,14,98	NPSC(L330)
14	IF (S(2)-999) 4,4,98	NPSC(L332)
4	ENUM=S(4)-S(2)	NPSC(L335)
	IF (A-S(1)) 99,5,5	NPSC(L340)
5	IF (A-S(3)) 6,6,100	NPSC(L345)
6	NPSC(L=(A-S(1))*ENUM/DEN+S(2)+.5	NPSC(L350)
	GO TO 101	NPSC(L355)
98	NPSC(L=-0	NPSC(L360)
	GO TO 101	NPSC(L365)
99	NPSC(L=0	NPSC(L370)
	GO TO 101	NPSC(L375)
100	NPSC(L=999	NPSC(L380)
101	RETURN	NPSC(L385)
	END(0,0,0,0,0)	

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
1	4	00055	2	6	00064	3	7	00070	14	8	00074
4	9	00100	5	11	00110	6	12	00114	98	14	00131
99	16	00134	100	18	00137	101	19	00141			

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
119	00167	32562	77462

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION, EQUIVALENCE OR COMMON SENTENCES

ENUM	DEC	OCT	DEC	OCT	DEC	OCT
118	00166	117	00165	NPSC	116	00164

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

64

PROPERTY IN SOURCE PROGRAM											
DEC		OCT		DEC		OCT		DEC		OCT	
9)	111	00157	2)	102	00146	3)	104	00150	6)	106	00152

APPENDIX E

PROGRAM DESCRIPTION - OUTPUT TAPE WRITE ROUTINE
NORTH AMERICAN AVIATION, INC. COLUMBUS
ENGINEERING PROGRAM DESCRIPTION

1. Identification

- a. Output Tape Write Routine, Deck - NCF WRITE.
- b. O. C. Juelich, June 1960.
- c. Research Group - 330.
- d. Fortran Source Deck is up to date.

2. Purpose

Writes up to ten floating point numbers per line retaining seven digit accuracy for most numbers.

3. Restrictions

- a. Writes output tape 6.
- b. Intended primarily for numbers between 10^{-3} and 10^7 in magnitude. Seven digit accuracy is retained for numbers between 1 and 10^7 .
- c. Source Deck includes 704 SAP instructions.

4. Method

A Format Statement is generated, using F conversion for numbers less than 10^7 and E conversion for numbers 10^7 or larger in magnitude.

5. Use

Reached through a Fortran Statement such as

CALL WRITE (6HiIDENT, A, N)

where i is the pre-print space control character

IDENT is the indicative word for the first line of print.

(The second line, if any, will be identified by an 11, the third by 21, etc.)

A is the first word to be printed.

N is the number of words to be printed, $N > 0$.

6. Coding Information

- a. This routine requires 171 locations.
- b. All inferior subroutines are part of the Fortran System.

SUBROUTINE WRITE(A,F,N)		WRITE000
SFMTA ALF (A6)		WRITE010
SFMTB ALF E10.2		WRITE020
SFMTF ALF F10.0		WRITE030
SFMTI ALF (I6)		WRITE040
SFMTX ALF)		WRITE050
DIMENSION F(25),FMT(12)		WRITE060
EQUIVALENCE (B,I8)		WRITE070
FMT(1)=FMTA		WRITE080
B=A		WRITE090
J=1		WRITE100
1	K=XMINOF(J+9,N)	WRITE110
	DO 2 I=J,K	WRITE120
	IT=I+2-J	WRITE130
	X=ABSF(F(I))	WRITE140
	L=-1	WRITE150
	DO 3 M=1,7	WRITE160
	IF (X-9 999 999A) 4,4,5	WRITE170
4	X=10*X	WRITE180
5	L=L+1	WRITE190
6	IF (L) 6,7,7	WRITE200
	FMT(IT)=FMTE	WRITE210
	GO TO 8	WRITE220
S7	CLA L	WRITE230
S	ARS 12	WRITE240
S	ORA FMTE	WRITE250
S	SLW FMT(IT)	WRITE260
8	FMT(IT+1)=FMTX	WRITE270
2	CONTINUE	WRITE280
	WRITE OUTPUT TAPE 6,FMT,B,(F(I),I=J,K)	WRITE290
9	IF (K-N) 9,10,9	WRITE300
	J=J+10	WRITE310
	IB=J	WRITE320
	FMT(1)=FMTI	WRITE330
	GO TO 1	WRITE340
10	RETURN	WRITE350
	CARDS	WRITE360

EXTERNAL FORMULA NUMBERS WITH CORRESPONDING INTERNAL FORMULA NUMBERS AND OCTAL LOCATIONS

EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC	EFN	IFN	LOC
1	12	00035	4	19	00077	3	20	00102	5	21	00112
6	22	00117	7	24	00122	8	28	00126	2	29	00130
9	38	00165	10	42	00175						

STORAGE NOT USED BY PROGRAM

DEC	OCT	DEC	OCT
171	00253	32562	77462

LOCATIONS OF NAMES IN TRANSFER VECTOR

(FIL)	DEC	OCT	(IOH)O	DEC	OCT	(LEV)	DEC	OCT	(STH)	DEC	OCT
	0	00000		2	00002		3	00003		1	00001

STORAGE LOCATIONS FOR VARIABLES APPEARING IN DIMENSION AND EQUIVALENCE SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
18	170 00252	FMT	169 00251	B	170 00252		

STORAGE LOCATIONS FOR VARIABLES NOT APPEARING IN DIMENSION, EQUIVALENCE OR COMMON SENTENCES

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
17	157 00235	I	156 00234	J	155 00233	K	154 00232
L	153 00231	M	152 00230	X	151 00227		

STORAGE LOCATIONS FOR SYMBOLS NOT APPEARING IN SOURCE PROGRAM

DEC	OCT	DEC	OCT	DEC	OCT	DEC	OCT
E18	91 00133	E18	77 00115	E16	71 00107	D1601	27 00033
D1407	73 00111	D1401	28 00034	C1200	150 00226	C162	149 00225
C161	148 00224	91	145 00221	11	146 00222	21	129 00201
31	138 00212	61	140 00214				

(LEV)	(IOH)O	(STH)	SUBROUTINES NOT PUNCHED FROM LIBRARY (FIL)
-------	--------	-------	--------------------------------------------

APPENDIX FSUMMARY OF LIBRARY ROUTINES

SQRT	Evaluates the square root of a non-negative floating-point number. Invokes ERROR if argument is less than zero.
COS	Evaluates the cosine of an angle expressed in radians in floating-point form.
SIN	Evaluates the sine of an angle expressed in radians in floating-point form.
EXP	Evaluates the exponential function (e^x) of a floating-point number less than 88. Invokes ERROR if the argument exceeds 88.
ERROR	<ol style="list-style-type: none">Produces a "back-trace" through the program, listing the point and subroutine at which the error was detected, the point at which the subroutine was called, up to the main program.Turns on the Divide Check indicator and tests the first instruction of the main program. If this is "IF DIVIDE CHECK" control goes to this statement, otherwise DUMP is invoked.
CHAIN	Loads a program identified by Record and Tape Number from Tape to Core and gives it control.
DUMP	Gives a full Memory Print-out and invokes EXIT.
EXIT	Returns control to the Monitor to end the job. (This function is also performed by the input tape reading system routine if an "End of File" is encountered on the input tape.)

APPENDIX G

SAMPLE INPUT AND OUTPUT

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____

DATE _____ PAGE _____ of _____ JOB NO. _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 3 2 .		TBL (1)	
13 5 1 8 . 6 8 8		T_0	$^{\circ}R$
25 2 1 1 6 . 2 1 6 9		P_0	lb/ft^2
37 1 7 1 6 . 4 8 2 7		R_0	$ft^2/sec^2 OR$
49 . 0 0 2 3 7 6 9 1 7	73	ρ_0	$slug/ft^3$
61 1 3 .	73	n	
1 3 7 .		TBL (6)	
13 - 5 0 0 . 0 1 1 9 7		h_{a1}	ft
25 3 6 0 8 9 . 2 3 8 8		h_{a2}	ft
37 8 2 0 2 0 . 9 9 7 3		h_{a3}	ft
49 1 5 4 1 9 9 . 4 7 5	73	h_{a4}	ft
61 1 7 3 8 8 4 . 5 1 4	73	h_{a5}	ft
1 4 2 .	2	TBL (11)	
13 2 5 9 1 8 6 . 3 5 1		h_{a6}	ft
25 2 9 5 2 7 5 . 5 9 0		h_{a7}	ft
37 3 4 4 4 8 8 . 1 8 8		h_{a8}	ft
49 5 2 4 9 3 4 . 3 8 2	73	h_{a9}	ft
61 5 5 7 7 4 2 . 7 8 1	73	h_{a10}	ft
1 4 7 .	3	TBL (16)	
13 6 5 6 1 6 7 . 9 7 8		h_{a11}	ft
25 1 2 8 3 0 0 0 .		h_{a12}	ft
37 2 6 2 3 2 8 9 . 0 6 3		h_{a13}	ft
49 1 7 1 6 . 4 8 2 7	73	R_{a1}	$ft^2/sec^2 OR$
61 1 7 1 6 . 4 8 2 7	73	R_{a2}	$ft^2/sec^2 OR$

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	OF	JOB NO.
1	NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH	
1	5 2 .		TBL (21)		
13	1 7 1 6 . 4 8 2 7		R _A 3		$ft^2/sec^2 \circ R$
25	1 7 1 6 . 4 8 2 7		R _A 4		$ft^2/sec^2 \circ R$
37	1 7 1 6 . 4 8 2 7		R _A 5		$ft^2/sec^2 \circ R$
49	1 7 1 6 . 4 8 2 7		R _A 6		$ft^2/sec^2 \circ R$
61	1 7 1 6 . 4 8 2 7		R _A 7		$ft^2/sec^2 \circ R$
1	5 7 .		TBL (26)		
13	1 7 1 6 . 4 8 2 7		R _A 8		$ft^2/sec^2 \circ R$
25	1 7 1 6 . 4 8 2 7		R _A 9		$ft^2/sec^2 \circ R$
37	1 7 1 6 . 4 8 2 7		R _A 10		$ft^2/sec^2 \circ R$
49	1 7 1 6 . 4 8 2 7		R _A 11		$ft^2/sec^2 \circ R$
61	1 7 1 6 . 4 8 2 7		R _A 12		$ft^2/sec^2 \circ R$
1	6 2 .		TBL (31)		
13	1 7 1 6 . 4 8 2 7		R _A 13		$ft^2/sec^2 \circ R$
25	5 2 0 . 4 7 1		T _A 1		$\circ R$
37	3 8 9 . 9 8 8		T _A 2		$\circ R$
49	3 8 9 . 9 8 8		T _A 3		$\circ R$
61	5 0 8 . 7 8 8		T _A 4		$\circ R$
1	6 7 .		TBL (36)		
13	5 0 8 . 7 8 8		T _A 5		$\circ R$
25	2 9 8 . 1 8 8		T _A 6		$\circ R$
37	2 9 8 . 1 8 8		T _A 7		$\circ R$
49	4 0 6 . 1 8 8		T _A 8		$\circ R$
61	2 3 8 6 . 1 8 8		T _A 9		$\circ R$

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____		PROGRAMMER _____		DATE _____		PAGE _____ of _____	JOB NO. _____
NUMBER		IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH				
1	7 2 .		TBL (41)				
13	2 5 6 6 . 1 8 8		T _B 10				°R
25	2 8 3 6 . 1 8 8		T _A 11				°R
37	4 0 3 9 . 8 5 6		T _A 12				°R
49	6 6 1 3 . 5 3 2 8	73	T _A 13	80			
61	1 . 4 0 1 1		γ _A 1	9			dimensionless
1	7 7 .		TBL (46)				
13	1 . 4 0 1 1		γ _A 2				dimensionless
25	1 . 4 0 1 1		γ _A 3				dimensionless
37	1 . 4 0 1 1		γ _A 4				dimensionless
49	1 . 4 0 1 1	73	γ _A 5	80			dimensionless
61	1 . 4 0 1 1		γ _B 6	1 0			dimensionless
1	8 2 .		TBL (51)				
13	1 . 4 0 1 1		γ _A 7				dimensionless
25	1 . 4 0 2 5		γ _A 8				dimensionless
37	1 . 4 1 9 5		γ _A 9				dimensionless
49	1 . 4 2 6 8	73	γ _A 10	80			dimensionless
61	1 . 4 5 4 5		γ _A 11	1 1			dimensionless
1	8 7 .		TBL (56)				
13	1 . 5 9 2 0		γ _A 12				dimensionless
25	1 . 6 5 8 3 4		γ _A 13				dimensionless
37	1 . 0 1 8 2 0 2 0		δ _A 1 A				dimensionless
49	0 .	73	x 10 ⁸				
51	. 2 2 3 3 5 8 8 5 8 7		δ _A 2 A	1 2			dimensionless

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	JOB NO.
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH		
1	9 2 .	TBL (61)			
13	0 .		$\times 10^8$		
25	. 2 4 5 6 0 5 2 3 1	δ_A 3 A			dimensionless
37	1 .		$\times 10^8$		
49	. 1 1 8 8 6 5 7 6	δ_A 4 A			dimensionless
61	2 .		$\times 10^8$		
1	9 7 .	TBL (66)			
13	. 5 7 5 5 7 3 3 4	δ_A 5 A			dimensionless
25	3 .		$\times 10^8$		
37	. 9 9 6 2 3 3 3 5	δ_A 6 A			dimensionless
49	5 .		$\times 10^8$		
61	. 1 0 3 0 6 9 4 2	δ_A 7 A			dimensionless
1	1 0 2 .	TBL (71)			
13	5 .		$\times 10^8$		
25	. 7 3 5 5 0 4 9 2	δ_A 8 A			dimensionless
37	7 .		$\times 10^8$		
49	. 3 5 7 2 6 2 5 5	δ_A 9 A			dimensionless
61	8 .		$\times 10^8$		
1	1 0 7 .	TBL (76)			
13	. 2 7 8 6 6 4 7 6	δ_A 10 A			dimensionless
25	8 .		$\times 10^8$		
37	. 1 4 0 6 7 3 9 1	δ_A 11 A			dimensionless
49	8 .		$\times 10^8$		
61	. 4 4 5 2 1 0 8 7	δ_A 12 A			dimensionless

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____		PROGRAMMER _____		DATE _____		PAGE _____ of _____		JOB NO. _____	
NUMBER		IDENTIFICATION		DESCRIPTION DO NOT KEY PUNCH					
1	112.			TBL (81)					
13	-10.			$\times 10^8$					
25	.36222			<i>dimensionless</i>					
37	-12.			$\times 10^8$					
49									
61									
1	28.			RECID					
13	22230100.								
25									
37	20902131.								
49	1.407698+16			$\mu = 1.407698 \times 10^{16}$					
61				<i>ft</i>					
1	7.								
13	.05			<i>degrees</i>					
25									
37	5.			<i>degrees</i>					
49									
61									
1	201.								
13	1.			<i>hi</i>					
25	0.			<i>i</i>					
37									
49									
61									
1				20					
13									
25									
37									
49									
61									

PORTION: FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____ JOB NO. _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 2 1 1 .			
13 1 .			
25 1 . 6 + 0 6		$h = 1.6 \times 10^6$	
37			
49			
61			
1 2 2 1 .			
13 2 .			
25 0 .			
37 . 0 2 5			
49			
61			
1 2 3 1 .			
13 1 .			
25 1 .			
37			
49			
61			
1 2 4 1 .			
13 1 .			
25 0 .			
37			
49			
61			

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____ JOB NO. _____

NUMBER		IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	- 2 5 1 .	73 80 2 5	Last Card of First Data Set.
13	1 .		h m
25	0 .		M
37			
49			
61			
1	- 2 8 .	73 80 2 6	Last Card of Second Data Set.
13	0 .		RECID = 0, Mark "end" on Tape 2
25			
37			
49			
61			
1	- 2 8 .	73 80 2 7	Last Card of Third Data Set.
13	- 1 .		RECID < 0, exit to Card-Punch Program via "CHAIN."
25			
37			
49			
61			
1	1 .	73 80 2 8	RECID
13	2 2 2 3 0 1 0 1 .		Wp
25	1 .		Wx
37	0 .		Wp
49	0 .		Wp
61	0 .		Wp

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PAGE	PAGE	of	JOB NO.	DESCRIPTION	DO NOT KEY PUNCH
1	6 .					
13	- 3 0 .				<i>f min</i>	
25	2 0 0 .				<i>C min</i>	
37	3 0 .				<i>f max</i>	
49	8 0 0 .				<i>C max</i>	
61	8 5 0 .				<i>C edge</i>	
1	1 1 .					
13	2 .				<i>F_f</i>	
25	0 .				<i>V min</i>	
37	1 0 0 .				<i>d min</i>	
49	3 6 0 .				<i>V max</i>	
61	8 2 0 .				<i>d max</i>	
1	- 1 6 .				Last Card of Data Set.	
13	8 5 0 .				<i>d edge</i>	
25	1 .				<i>F_r</i>	
37	0 .				CID (not ready to punch cards)	
49						
61						
1	2 .					
13	0 .				<i>w_p</i>	
25	1 .				<i>w_r</i>	
37						
49						
61						
1						
13						
25						
37						
49						
61						
1						
13						
25						
37						
49						
61						

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____ JOB NO. _____

NUMBER		IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	1 1 .		
13	3 .		
25			
37			
49			
61			
1	- 1 7 .		
13	0 .		
25			
37			
49			
61			
1			
13			
25			
37			
49			
61			
1			
13			
25			
37			
49			
61			
1			
13			
25			
37			
49			
61			

Last Card of Data Set

Fr (do not punch r - same argument field as before)

PARAMETER LIST -

OI =	0.
HP =	1600000.
EC =	0.
	0.025000
GAM =	1.000
GAMQ =	0.
OM =	0.

OI
0.

HP
160000.

EC
0.

GAM
1.0000E 00

GAMQ
0.

OM
0.

D PHI MIN
5.0000E-02

D PHI PRINT
5.0000E 00

RECORD ID
22230100.

PHI	H	RHO	GAMMA	ALPHA H1	ALPHA H2	ALPHA PA	N
5.000	160000.	5.0380E-15	0.	0.996	4.993	-0.	8
10.000	160000.	5.0390E-15	0.	0.983	9.944	0.	1
15.000	160000.	5.0380E-15	0.	0.962	14.810	-0.	1
20.000	160000.	5.0380E-15	0.	0.933	19.551	0.	1
25.000	160000.	5.0380E-15	0.	0.896	24.126	-0.	1
30.000	160000.	5.0380E-15	0.	0.851	28.497	0.	1
35.000	160000.	5.0380E-15	0.	0.799	32.626	-0.	1
40.000	160000.	5.0380E-15	0.	0.741	36.479	0.	1
45.000	160000.	5.0380E-15	0.	0.676	40.022	-0.	1
50.000	160000.	5.0380E-15	0.	0.605	43.227	0.	1
55.000	160000.	5.0380E-15	0.	0.529	46.065	-0.	1
60.000	160000.	5.0380E-15	0.	0.449	48.512	0.	1
65.000	160000.	5.0380E-15	0.	0.365	50.549	-0.	10
70.000	160000.	5.0380E-15	0.	0.278	52.157	0.	1
75.000	160000.	5.0380E-15	0.	0.188	53.323	-0.	1
80.000	160000.	5.0380E-15	0.	0.097	54.037	0.	1
85.000	160000.	5.0380E-15	0.	0.005	54.294	-0.	1
90.000	160000.	5.0380E-15	0.	-0.087	54.090	0.	1
95.000	160000.	5.0380E-15	0.	-0.178	53.428	-0.	1
100.000	160000.	5.0380E-15	0.	-0.268	52.313	0.	1
105.000	160000.	5.0380E-15	0.	-0.355	50.755	-0.	1
110.000	160000.	5.0380E-15	0.	-0.440	48.766	0.	1
115.000	160000.	5.0380E-15	0.	-0.520	46.364	-0.	1
120.000	160000.	5.0380E-15	0.	-0.597	43.570	0.	1
125.000	160000.	5.0380E-15	0.	-0.668	40.406	-0.	1
130.000	160000.	5.0380E-15	0.	-0.734	36.900	0.	1
135.000	160000.	5.0380E-15	0.	-0.793	33.081	-0.	1
140.000	160000.	5.0380E-15	0.	-0.846	28.981	0.	1
145.000	160000.	5.0380E-15	0.	-0.891	24.636	-0.	1
150.000	160000.	5.0380E-15	0.	-0.929	20.083	0.	1
155.000	160000.	5.0380E-15	0.	-0.959	15.359	-0.	1
160.000	160000.	5.0380E-15	0.	-0.981	10.505	0.	1
165.000	160000.	5.0380E-15	0.	-0.995	5.562	-0.	1
170.000	160000.	5.0380E-15	0.	-1.000	0.571	0.	1
175.000	160000.	5.0380E-15	0.	-0.997	-4.424	-0.	1
180.000	160000.	5.0380E-15	0.	-0.985	-9.381	0.	1

185.000	1600000.	5.0380E-15	-0.	-0.965	-14.259	-0.	1
190.000	1600000.	5.0380E-15	-0.	-0.937	-19.017	-0.	1
195.000	1600000.	5.0380E-15	-0.	-0.900	-23.613	-0.	1
200.000	1600000.	5.0380E-15	-0.	-0.857	-28.009	-0.	1
205.000	1600000.	5.0380E-15	-0.	-0.806	-32.167	-0.	1
210.000	1600000.	5.0380E-15	-0.	-0.748	-36.053	-0.	1
215.000	1600000.	5.0380E-15	-0.	-0.683	-39.634	-0.	1
220.000	1600000.	5.0380E-15	-0.	-0.613	-42.878	-0.	1
225.000	1600000.	5.0380E-15	-0.	-0.538	-45.760	-0.	1
230.000	1600000.	5.0380E-15	-0.	-0.458	-48.253	-0.	1
235.000	1600000.	5.0380E-15	-0.	-0.375	-50.338	-0.	1
240.000	1600000.	5.0380E-15	-0.	-0.288	-51.995	-0.	1
245.000	1600000.	5.0380E-15	-0.	-0.199	-53.213	-0.	1
250.000	1600000.	5.0380E-15	-0.	-0.108	-53.979	-0.	1
255.000	1600000.	5.0380E-15	-0.	-0.016	-54.288	-0.	1
260.000	1600000.	5.0380E-15	-0.	0.076	-54.137	-0.	1
265.000	1600000.	5.0380E-15	-0.	0.168	-53.527	-0.	1
270.000	1600000.	5.0380E-15	-0.	0.258	-52.463	-0.	1
275.000	1600000.	5.0380E-15	-0.	0.345	-50.955	-0.	1
280.000	1600000.	5.0380E-15	-0.	0.430	-49.015	-0.	1
285.000	1600000.	5.0380E-15	-0.	0.511	-46.659	-0.	1
290.000	1600000.	5.0380E-15	-0.	0.588	-43.908	-0.	1
295.000	1600000.	5.0380E-15	-0.	0.660	-40.785	-0.	1
300.000	1600000.	5.0380E-15	-0.	0.726	-37.317	-0.	1
305.000	1600000.	5.0380E-15	-0.	0.786	-33.532	-0.	1
310.000	1600000.	5.0380E-15	-0.	0.840	-29.463	-0.	1
315.000	1600000.	5.0380E-15	-0.	0.886	-25.144	-0.	1
320.000	1600000.	5.0380E-15	-0.	0.925	-20.612	-0.	1
325.000	1600000.	5.0380E-15	-0.	0.956	-15.906	-0.	1
330.000	1600000.	5.0380E-15	-0.	0.979	-11.065	-0.	1
335.000	1600000.	5.0380E-15	-0.	0.994	-6.130	-0.	1
340.000	1600000.	5.0380E-15	-0.	1.000	-1.143	-0.	1
345.000	1600000.	5.0380E-15	-0.	0.997	3.854	-0.	1
350.000	1600000.	5.0380E-15	-0.	0.987	8.818	-0.	1
355.000	1600000.	5.0380E-15	-0.	0.968	13.707	-0.	1
360.000	1600000.	5.0380E-15	-0.	0.940	18.481	-0.	1

OI	HP	EC	GAM	GAMQ	OM	
0.	160000.	0.	1.0000E 00	0.	0.	
D PHI MIN	D PHI PRINT					
5.0000E-02	5.0000E 00					
		DELTA	END DERIVATIVES			NT
		1.1942E-01	-0.006	0.940	-0.	79
	TH PER BD	WEIGHT THETA H1	MAX THETAS	54.294	0.	
	0.	0.	1.000			
	WEIGHT THETA H2		MAX DERIVATIVES	1.000	0.	
	-0.		0.018			

OI
0.
D PHI MIN
5.0000E-02
HP
160000.
D PHI PRINT
5.0000E 00

EC
0.0250C0

GAM
1.0000E 00

GAMQ
0.

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RECORD ID
22230101.

PHI	H	RHO	GAMMA	ALPHA H1	ALPHA H2	ALPHA PA	N
5.000	1602088.	4.9958E-15	0.122	0.874	4.871	-0.122	8
10.000	1608341.	4.8720E-15	0.243	0.740	9.704	-0.244	1
15.000	1618717.	4.6739E-15	0.362	0.600	14.460	-0.366	1
20.000	1633147.	4.4132E-15	0.479	0.455	19.108	-0.488	1
25.000	1651539.	4.1042E-15	0.592	0.307	23.621	-0.611	1
30.000	1673771.	3.7625E-15	0.701	0.156	27.978	-0.734	1
35.000	1699695.	3.4034E-15	0.805	0.005	32.167	-0.859	1
40.000	1729139.	3.0412E-15	0.903	-0.145	36.183	-0.986	1
45.000	1761906.	2.6879E-15	0.995	-0.293	40.024	-1.115	1
50.000	1797773.	2.3527E-15	1.080	-0.438	43.695	-1.247	1
55.000	1836495.	2.0423E-15	1.157	-0.577	47.207	-1.384	1
60.000	1877804.	1.7606E-15	1.225	-0.710	50.569	-1.525	1
65.000	1921412.	1.5095E-15	1.285	-0.836	53.795	-1.672	1
70.000	1967010.	1.2889E-15	1.335	-0.954	56.900	-1.825	1
75.000	2014273.	1.0975E-15	1.375	-1.063	59.896	-1.985	1
80.000	2062857.	9.3334E-16	1.405	-1.162	62.797	-2.152	1
85.000	2112407.	7.9366E-16	1.424	-1.252	65.616	-2.328	1
90.000	2162553.	6.7569E-16	1.432	-1.332	68.364	-2.512	1
95.000	2212918.	5.7662E-16	1.430	-1.401	71.051	-2.705	1
100.000	2263118.	4.9379E-16	1.417	-1.460	73.686	-2.907	1
105.000	2312764.	4.2478E-16	1.393	-1.508	76.277	-3.117	1
110.000	2361468.	3.6743E-16	1.358	-1.546	78.830	-3.337	1
115.000	2408844.	3.1985E-16	1.312	-1.573	81.351	-3.565	1
120.000	2454511.	2.8044E-16	1.256	-1.589	83.844	-3.802	1
125.000	2498098.	2.4785E-16	1.190	-1.597	86.312	-4.047	1
130.000	2539249.	2.2094E-16	1.115	-1.594	88.760	-4.300	1
135.000	2577620.	1.9877E-16	1.031	-1.583	91.187	-4.560	1
140.000	2612891.	1.8058E-16	0.939	-1.564	93.597	-4.826	8
145.000	2644765.	1.6574E-16	0.839	-1.537	95.989	-5.099	2
150.000	2672969.	1.5375E-16	0.732	-1.503	98.365	-5.376	1
155.000	2697260.	1.4420E-16	0.619	-1.463	100.722	-5.658	1
160.000	2717431.	1.3677E-16	0.502	-1.418	103.063	-5.943	1
165.000	2733305.	1.3123E-16	0.380	-1.369	105.384	-6.231	1
170.000	2744744.	1.2739E-16	0.255	-1.317	107.685	-6.520	1
175.000	2751647.	1.2514E-16	0.128	-1.262	109.964	-6.810	1
180.000	2753955.	1.2439E-16	0.000	-1.206	112.220	-7.099	1

185.000	2751647.	1.2514E-16	-0.128	-1.150	114.450	-7.386	1
190.000	2744744.	1.2739E-16	-0.255	-1.095	116.651	-7.671	1
195.000	2733305.	1.3123E-16	-0.380	-1.041	118.821	-7.952	1
200.000	2717431.	1.3677E-16	-0.502	-0.990	120.957	-8.228	1
205.000	2697261.	1.4420E-16	-0.619	-0.942	123.055	-8.498	1
210.000	2672969.	1.5375E-16	-0.732	-0.899	125.112	-8.760	1
215.000	2644765.	1.6574E-16	-0.839	-0.862	127.124	-9.015	1
220.000	2612892.	1.8058E-16	-0.939	-0.830	129.085	-9.260	1
225.000	2577620.	1.9877E-16	-1.031	-0.805	130.992	-9.495	1
230.000	2539249.	2.2094E-16	-1.115	-0.788	132.837	-9.718	1
235.000	2498099.	2.4785E-16	-1.190	-0.779	134.614	-9.928	1
240.000	2454511.	2.8044E-16	-1.256	-0.777	136.316	-10.125	1
245.000	2408844.	3.1985E-16	-1.312	-0.785	137.933	-10.306	1
250.000	2361469.	3.6742E-16	-1.358	-0.801	139.454	-10.471	1
255.000	2312765.	4.2478E-16	-1.393	-0.826	140.867	-10.619	1
260.000	2263118.	4.9379E-16	-1.417	-0.860	142.158	-10.747	1
265.000	2212918.	5.7662E-16	-1.430	-0.903	143.308	-10.855	1
270.000	2162553.	6.7569E-16	-1.432	-0.954	144.297	-10.940	1
275.000	2112408.	7.9366E-16	-1.424	-1.013	145.100	-11.001	1.84
280.000	2062858.	9.3333E-16	-1.405	-1.079	145.688	-11.036	1
285.000	2014274.	1.0975E-15	-1.375	-1.151	146.025	-11.041	1
290.000	1967011.	1.2889E-15	-1.335	-1.229	146.074	-11.015	1
295.000	1921412.	1.5095E-15	-1.285	-1.310	145.787	-10.953	1
300.000	1877804.	1.7606E-15	-1.225	-1.394	145.114	-10.853	1
305.000	1836495.	2.0423E-15	-1.157	-1.479	143.997	-10.711	1
310.000	1797773.	2.3527E-15	-1.080	-1.563	142.373	-10.523	1
315.000	1761906.	2.6879E-15	-0.995	-1.644	140.176	-10.284	1
320.000	1729140.	3.0412E-15	-0.903	-1.720	137.340	-9.991	1
325.000	1699695.	3.4034E-15	-0.805	-1.789	133.799	-9.639	1
330.000	1673771.	3.7624E-15	-0.701	-1.849	129.492	-9.227	1
335.000	1651539.	4.1042E-15	-0.592	-1.898	124.369	-8.750	1
340.000	1633147.	4.4132E-15	-0.479	-1.934	118.392	-8.210	1
345.000	1618717.	4.6739E-15	-0.362	-1.955	111.543	-7.605	1
350.000	1608341.	4.8720E-15	-0.243	-1.961	103.824	-6.937	1
355.000	1602088.	4.9958E-15	-0.122	-1.950	95.259	-6.212	1
360.000	1600000.	5.0380E-15	-0.000	-1.923	85.897	-5.434	1

OI	HP	EC	GAM	GAMQ	OM	
0.	160000.	0.0250C0	1.0000E 00	0.	0.	
D PHI MIN	D PHI PRINT				RECORD ID	
5.0000E-02	5.0000E 00				22230101.	
		DELTA		END DERIVATIVES		NT
		5.8469E 0C		0.031	-1.923	87
	TH PER BD	WEIGHT THETA H1				
	2.1596E 01	-8.7613E-07		MAX THETAS		
				2.643	144.739	12.440
		WEIGHT THETA H2		MAX DERIVATIVES		
		6.3257E-02		0.031	1.923	0.185

TAPE RECORD		WEIGHT PAR		WEIGHT GAMMA		WEIGHT HI		WEIGHT H2		CARD FIELD	
22230101.		0.		1.000000E 00		0.		0.		3.	
SCALING -	MIN VALUE	MIN COUNTS	MAX VALUE	MAX COUNTS	EDGE COUNTS	EDGE COUNTS	EDGE COUNTS	EDGE COUNTS	EDGE COUNTS	EDGE COUNTS	EDGE COUNTS
FUNCTION	-30.000	200.	50.000	800.	850.	850.	850.	850.	850.	850.	850.
ARGUMENT	0.	100.	360.000	820.	820.	820.	820.	820.	820.	820.	820.
DECK ID -	0.										
D WHS	5.846886	-0.000001	0.063257								
FNCTN	0.	0.121808	0.242756	0.361990	0.478663	0.591944	0.701020	0.805100	0.903424	0.995262	
11	1.079924	1.156762	1.225175	1.284618	1.334599	1.374692	1.404536	1.423841	1.432394	1.430060	
21	1.416784	1.392598	1.357619	1.312053	1.256192	1.190419	1.115199	1.031083	0.938703	0.838765	
31	0.732047	0.619390	0.501694	0.379905	0.255012	0.128031	0.000001	-0.128029	-0.255010	-0.379904	
41	-0.501693	-0.619389	-0.732046	-0.828764	-0.938702	-1.031082	-1.115198	-1.190418	-1.256192	-1.312052	
51	-1.357619	-1.392597	-1.416784	-1.423060	-1.432394	-1.423842	-1.404536	-1.374692	-1.334599	-1.284618	
61	-1.225176	-1.156762	-1.079925	-0.995263	-0.903425	-0.805101	-0.701021	-0.591945	-0.478664	-0.361991	
71	-0.242757	-0.121809	-0.000001								

BIBLIOGRAPHY

1. Minzner, R. A., "Higher Atmospheric Densities and Temperatures Demanded by Satellite and Recent Rocket Measurements", American Rocket Society Preprint Number 781-59.
2. Coddington, E. A. and Levinson, N., Theory of Ordinary Differential Equations, McGraw-Hill, New York, 1955, pp. 218-220.
3. Gill, S., "A Process for the Step-by-Step Integration of Differential Equations in an Automatic Digital Computing Machine", Proceedings of the Cambridge Philosophical Society, Volume 47, 1951, pp. 96 to 108.
4. Milne, W. E., Numerical Calculus, Princeton University Press, Princeton, 1949.
5. Milne, W. E., Numerical Solution of Differential Equations, John Wiley & Sons, Inc., New York, 1953.
6. The Fortran Automatic Coding System for the IBM 704 EDPM, International Business Machines Corporation, New York, 1956.
7. Reference Manual - Fortran II - for the IBM 704 Data Processing System, International Business Machines Corporation, New York, 1958.